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A11106 064743



# NBS SPECIAL PUBLICATION **400-64**

**REFERENCE**

NBS  
PUBLICATIONS

U.S. DEPARTMENT OF COMMERCE / National Bureau of Standards

## *Semiconductor Measurement Technology:*

The Relationship Between Resistivity  
and Dopant Density for Phosphorus-  
and Boron-Doped Silicon

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#400-64  
1981

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*Semiconductor Measurement Technology:*

## **The Relationship Between Resistivity and Dopant Density for Phosphorus- and Boron-Doped Silicon**

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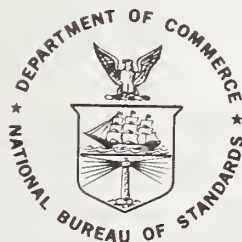
Statistical Engineering Division  
Center for Applied Mathematics  
National Engineering Laboratory  
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This activity was supported by:

Defense Advanced Research Projects Agency  
1400 Wilson Boulevard  
Arlington, VA 22209

and

National Bureau of Standards  
Washington, DC 20234



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U.S. DEPARTMENT OF COMMERCE, Malcolm Baldrige, Secretary  
NATIONAL BUREAU OF STANDARDS, Ernest Ambler, Director

Issued May 1981

Library of Congress Catalog Card Number: 81-600052

**National Bureau of Standards Special Publication 400-64**

Nat. Bur. Stand. (U.S.), Spec. Publ. 400-64, 53 pages (May 1981)

CODEN: XNBSAV

U.S. GOVERNMENT PRINTING OFFICE  
WASHINGTON: 1981

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For sale by the Superintendent of Documents, U.S. Government Printing Office, Washington, D.C. 20402

Price \$3.25

(Add 25 percent for other than U.S. mailing)

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*Semiconductor Measurement Technology:*  
The Relationship Between Resistivity and Dopant Density for  
Phosphorus- and Boron-Doped Silicon\*

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New data have been obtained for the resistivity-dopant density relationship for silicon doped with phosphorus or boron for dopant densities in the range  $10^{13}$  to  $10^{20}$   $\text{cm}^{-3}$ . For dopant densities less than  $10^{18}$   $\text{cm}^{-3}$ , results were calculated from resistivity and junction capacitance-voltage measurements on processed wafers. For more heavily doped material, data were obtained from Hall effect and resistivity measurements on specimens cut from bulk silicon slices. These primary methods were supplemented for phosphorus-doped material by neutron activation analysis and a photometric technique and for boron-doped material by the nuclear track technique. For phosphorus-doped silicon the results of this work differ by 5 to 15 percent from the commonly used Irvin curve, always in the direction of lower resistivity for a given dopant density. For boron-doped silicon the results differ significantly from the *p*-type Irvin curve for boron densities greater than  $10^{16}$   $\text{cm}^{-3}$  with a maximum deviation of 45 percent at  $5 \times 10^{17}$   $\text{cm}^{-3}$  in the direction of lower resistivity for a given dopant density. Hole mobility values derived from the data are in reasonable agreement with the Wagner expression with a maximum discrepancy of 10 percent in the  $10^{18}$   $\text{cm}^{-3}$  range. Analytical curves were fitted to the resistivity-dopant density product as a function of resistivity and dopant density for temperatures of both 23°C and 300 K. Similar curves were obtained for the calculated carrier mobility as a function of resistivity and carrier density.

*Key Words:* Boron; capacitance-voltage technique; dopant density; electron mobility; Hall effect; hole mobility; Irvin curves; phosphorus; resistivity; semiconductor; silicon.

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\* This work was conducted as part of the Semiconductor Technology Program at NBS and was supported in part by the Defense Advanced Research Projects Agency (Order No. 2397).

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## 1. INTRODUCTION

The conversion between resistivity and dopant density of silicon is widely used in the semiconductor industry. In device design, the calculation of various parameters such as breakdown voltage involves relating resistivity, which can be readily measured, to dopant density, which is the desired quantity but very difficult to measure directly. Applications using the conversion over many decades of dopant density include the calculation of the surface dopant density of a diffused layer from the sheet resistance-junction depth product and the determination of a dopant density profile from incremental sheet resistance measurements. Significant error in the results of these measurements occurs when incorrect expressions are used to relate resistivity and dopant density.

During the past decade, the most frequently used conversion curves for both *n*- and *p*-type silicon are those formulated by Caughey and Thomas [1] based on the curves of Irvin [2]. Irvin's curve for *n*-type material includes measurements on silicon doped with arsenic, antimony, and phosphorus. More recently Baccarani and Ostojica [3] published a conversion for phosphorus-doped silicon which agrees with that of Irvin at low phosphorus densities but departs at high densities in the direction of lower resistivity for a given phosphorus density with a difference of 30 percent at  $10^{20}$  cm<sup>-3</sup>. Irvin's curve for *p*-type material includes measurements on silicon doped with aluminum, gallium, and boron. More recently Wagner [4] published a conversion for boron-doped silicon based on ion implantation results which differs from that of Irvin by up to 50 percent (in the direction of lower resistivity for a given boron density) for densities in the range  $10^{16}$  to  $10^{18}$  cm<sup>-3</sup>. This report describes the results of a comprehensive redetermination of the resistivity-dopant density relationships for both phosphorus-doped silicon and boron-doped silicon and documents the results of the measurements upon which the redetermination was made. Papers have been published which summarize the results of this work on silicon doped with phosphorus [5] and with boron [6], but these papers do not contain either a complete record of the measurements used for the redetermination or a comprehensive discussion of many of the experimental and analytical details, both of which are included in this report.

## 2. MATERIAL SELECTION

The starting material, in both ingot and slice form, was obtained from several different suppliers and was selected for minimum resistivity gradients by mechanical four-probe array measurements [7] prior to use. For phosphorus-doped silicon, most of the results on high resistivity material were obtained on neutron transmutation doped silicon which proved much more uniform than material doped by more conventional techniques. The difference between center and half radius resistivity values ranged from -3 percent to +7 percent with an average absolute difference of +2.5 percent for the selected phosphorus-doped material and even less for the selected boron-doped material. Spreading resistance measurements were made on a number of ingots and slices to check on fine structure in the resistivity. All of the boron-doped material was very uniform, but a slight fine structure with a period of about 1 mm and a peak-to-valley variation of about 15 percent was seen in some of the phosphorus-doped material.





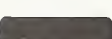

### 3. TEST STRUCTURE MEASUREMENTS

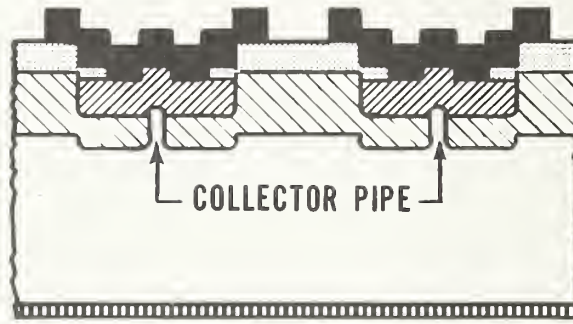
For dopant densities of  $10^{18}$   $\text{cm}^{-3}$  or less, resistivity and dopant density data were obtained from microelectronic test structures fabricated on silicon slices. The resistivity was measured directly on planar four-probe square array structures described in detail elsewhere [8]. A cross-sectional view of this structure is shown in figure 1. The dopant density was determined from capacitance-voltage (C-V) measurements [9] on gated  $p$ - $n$  junction diodes. These test structures and other diagnostic structures were assembled on microelectronic test patterns NBS-3 [10] and NBS-4 [11] which were prepared especially for this work.

The patterns were fabricated on the silicon slices by bipolar processing [12]. Various measurements were made on the wafers to verify the fabrication and to assure that leakage currents were low enough for proper operation of the test structures. The resistivity data obtained from the square array structures agreed to within a few percent with mechanical four-probe measurements [13] made prior to fabrication.

The dopant density was measured by the C-V method [9] on the gated base-collector diode structure shown schematically in figure 2. This method gives the net dopant density, i.e., the number of dopant atoms in excess of any compensating atoms on the more lightly doped side of the junction. For meaningful C-V measurements, it is important to bias the gate at the flat-band voltage which was determined from  $C_{\text{min}} - C_{\text{max}}$  measurements on an MOS capacitor structure of the test pattern [14]. The dopant density calculated from the C-V method is particularly sensitive to the value used for the diameter of the diode as the diameter enters as the fourth power. The diameter (nominally 432  $\mu\text{m}$ ) of several diodes was measured by the NBS line-standard scanning interferometer [15]. These results were then used as a calibration for determining from photomicrographs the diameters of other diodes from each processing run of wafers. The uncertainty in the measured diameter is estimated to be less than 1  $\mu\text{m}$ . The base junction depth, used in the analysis of the C-V data, was measured by the groove and stain technique [16] with an estimated error of  $\pm 0.1$   $\mu\text{m}$ .

Dopant density values were calculated from the C-V data using a computer program which includes corrections for peripheral effects and takes into account the fraction of the total depletion depth which occurs in the diffused layer [17]. A fitting procedure [18] was incorporated into the program in which a Gaussian shape is assumed for the base diffusion near the junction, and the surface concentration of the diffusion and the background dopant density are adjusted to give a best fit to all the C-V data. The fitting procedure made it possible to obtain results on wafers with dopant densities up to  $7 \times 10^{17}$   $\text{cm}^{-3}$ ; otherwise, wafers with dopant density greater than  $10^{17}$   $\text{cm}^{-3}$  could not be measured because of compensation by the diffusion tail within the depletion depth obtainable in the substrate before voltage breakdown occurs. This fitting procedure was used for reducing the C-V data to dopant density for all wafers except a few of the lightly doped ones. For these lightly doped wafers, the program was used without the iterative fitting procedure as the diffused layer effects are negligible. Some lightly doped wafers were analyzed both ways, and the dopant density values were the same with the

-  COLLECTOR
-  EMITTER
-  BASE
-  OXIDE
-  ALUMINUM
-  GOLD



→ | 25 μ m | ←

Figure 1. Schematic cross-sectional view of the four-probe resistor test structure. The pipes are arranged in a square configuration with a center-to-center spacing of 57.2 μm (2.25 mil).

fitting procedure as without. In the calculations, a value of 11.7 [19] was used for the relative dielectric constant of silicon.

The square array resistivity results were corrected to both 23°C and 300 K from the actual measurement temperatures using published coefficients for the change of resistivity with temperature [20]. The measurement temperature was determined by a copper-constantan thermocouple imbedded in the vacuum chuck holding the wafer on a probe station. The C-V measurements were made at room temperature with no correction for temperature as the dopant is completely ionized in the depletion layer.

The procedure used for correlating the resistivity and dopant density values was slightly different for the two test patterns. The one four-probe resistor structure contained on test pattern NBS-3 is not located in the same cell as the diode used for the dopant density measurements. In order to minimize the influence of resistivity variations over the wafer, the average of the resistivities measured on the two four-probe resistors on either side of the diode was taken as the resistivity corresponding to the dopant density at that diode site. On test pattern NBS-4, there are four four-probe resistor structures with different collector pipe sizes for measuring a wide range of resistivities in the cell containing the base-collector diode. On this pattern, an average resistivity was obtained from measurements on two or more adjacent four-probe structures in the cell containing the diode. Differences between minimum and maximum values of resistivity in a given cell rarely exceeded 1 percent for boron-doped material but were in the range from 1 to 5 percent for phosphorus-doped material because of the localized resistivity variations characteristic of most phosphorus-doped silicon. Typically, for wafers fabricated with either test pattern, data were collected for six cells near the center of each wafer and the results averaged. Mobility values calculated for a few of the wafers were judged significantly below those from other wafers with similar dopant densities. The wafers with low mobility were omitted from the results so that the curves would represent good material without appreciable compensation or other problems.

The estimated error in the planar four-probe resistivity measurements is about 1 percent. Factors which contribute to the error are finite wafer thickness, pipe spacing uncertainty, instrument calibration, and temperature measurement. Errors in the dopant density due to uncertainties in the surface dopant density of the diffusion, junction depth, and random measurement error were examined in idealized data studies [18]. The errors caused by uncertainties in these parameters for the wafers in this work were shown to be less than one percent. Additional error in the dopant density arises from uncertainties in diode diameter, flat-band voltage, and instrument calibration, giving a total estimated error of 2 percent. Resistivity gradients in the wafers are an additional source of error in that the resistivity at the diode site may be different from that measured at the four-probe sites as discussed above. Consequently, for phosphorus-doped material, even after averaging over six sites, the total error may be as large as 5 percent. For the more uniform boron-doped material, the total error is in the range of 3 percent.



Figure 2. Cross-sectional view of the base-collector diode used for the junction C-V measurements of dopant density.

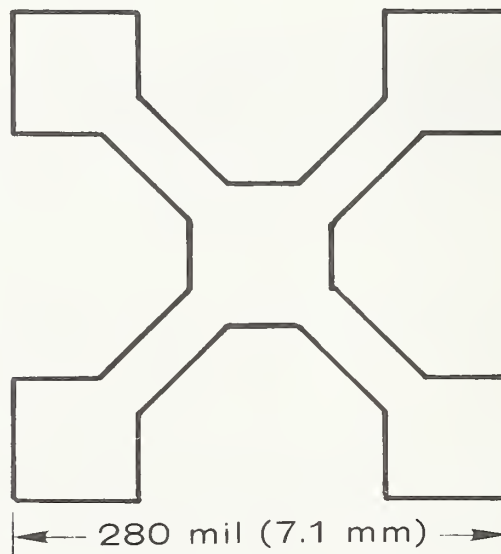


Figure 3. Shape of van der Pauw specimens ultrasonically cut from bulk silicon slices.

#### 4. HALL EFFECT MEASUREMENTS

For dopant densities greater than  $10^{19} \text{ cm}^{-3}$ , Hall effect and resistivity measurements were made on van der Pauw specimens [21] ultrasonically cut from bulk silicon slices. The shape of the specimens is shown in figure 3. For selected slices, a Greek cross design [22] was also cut. The measurements were made at controlled temperatures of both  $23^\circ\text{C}$  and  $300 \text{ K}$  for a magnetic flux density of  $0.6 \text{ T}$  ( $6 \text{ kG}$ ) following standard procedures [23]. The commercial Hall probe for measuring the flux density was calibrated using an NMR gaussmeter. The integrating digital voltmeter used for all the voltage measurements was calibrated using a standard voltage source and a standard cell calibrated at NBS. The standard resistors used for the determination of the current through the specimens were calibrated against other standard resistors with known values. Resistivity values obtained from the van der Pauw specimens were within a few percent of the four-probe values measured on the respective wafers during the material selection process.

For phosphorus-doped silicon the electron density,  $n$ , was calculated from the expression  $n = -r/qR_H$ , where  $q$  is the electronic charge,  $R_H$  is the Hall coefficient, and  $r$  is the Hall scattering factor [24]. For heavily doped  $n$ -type material,  $r$  is unity.

For boron-doped silicon the hole density,  $p$ , was calculated from the expression  $p = r/qR_H$ . Due to the complex nature of the valence band of silicon, the factor  $r$  for  $p$ -type material is less than unity, even for heavily doped specimens. In this work  $r$  was taken equal to  $0.8$  as the majority of experimental results [25-28] and recent calculations [29] on moderately doped material suggest a value in this range. No measurements of  $r$  for dopant densities greater than  $2 \times 10^{18} \text{ cm}^{-3}$  appear to be available for  $p$ -type silicon.

Results obtained on the van der Pauw specimens have an estimated error of less than 3 percent for phosphorus-doped material. Most of this error is in the Hall coefficient as it is more difficult to measure accurately than is the resistivity. The measurement-related error is the same for boron-doped material, but the uncertainty in  $r$  contributes an additional, unknown error. There is the probability that  $r$  differs from  $0.8$  by  $\pm 0.1$ . This corresponds to an error of up to 15 percent in  $p$ .

#### 5. RESULTS FOR PHOSPHORUS-DOPED SILICON

Table 1 gives the data for phosphorus-doped silicon obtained from measurements on test patterns. Under wafer identification in column 1 are listed: (1) the wafer number, (2) the initial resistivity at  $23^\circ\text{C}$  from four-probe array measurements at the center of the wafer before processing, (3) the test pattern used for fabrication, and (4) the measured diameter,  $D$ , in micrometers of the diodes used for the C-V measurements of dopant density,  $N$ , in column 3. The site listed in column 2 gives the x-y coordinates of the diode on the wafer. The diode in the approximate center of the wafer is designated 0,0 and the others are referenced with respect to it. For example -1,1 specifies the diode located one unit (200 mils) in the -x direction and one unit in the +y direction from the reference diode. Columns 4 and 5 give the resistivity values measured using the four-probe resistor structures and corrected to  $23^\circ\text{C}$  and  $300 \text{ K}$ , respectively. Column 6 gives the electron density

Table 1. Data for Phosphorus-Doped Silicon Obtained from Test Patterns.

| Wafer Identification                              | Site                     | N<br>cm <sup>-3</sup>    | $\rho_{23^\circ\text{C}}$<br>$\Omega\cdot\text{cm}$ | $\rho_{300\text{ K}}$<br>$\Omega\cdot\text{cm}$ | n<br>cm <sup>-3</sup>    | $\mu_{23^\circ\text{C}}$<br>cm <sup>2</sup> /V·s | $\mu_{300\text{ K}}$<br>cm <sup>2</sup> /V·s |
|---|--------------------------|--------------------------|---|---|--------------------------|--|--|
| G140Ph-1<br>$\rho_i = 137$<br>NBS-4<br>D = 433.3  | 0,0                      | 2.699 x 10 <sup>13</sup> | 158.3   | 163.3   | 2.699 x 10 <sup>13</sup> | 1461   | 1413   |
|   | -1,0                     | 2.691 x 10 <sup>13</sup> | 158.8   | 163.9   | 2.691 x 10 <sup>13</sup> | 1461   | 1415   |
|   | -1,1                     | 2.598 x 10 <sup>13</sup> | 159.0   | 164.1   | 2.598 x 10 <sup>13</sup> | 1511   | 1464   |
|   | 0,1                      | 2.671 x 10 <sup>13</sup> | 158.7   | 163.8   | 2.671 x 10 <sup>13</sup> | 1472   | 1427   |
|   | 1,1                      | 2.790 x 10 <sup>13</sup> | 158.4   | 163.4   | 2.790 x 10 <sup>13</sup> | 1412   | 1369   |
|   | 1,0                      | 2.757 x 10 <sup>13</sup> | 158.1   | 163.2   | 2.757 x 10 <sup>13</sup> | 1432   | 1387   |
|   | Avg.                     | 2.701 x 10 <sup>13</sup> | 158.6   | 163.6   | 2.701 x 10 <sup>13</sup> | 1458 ± 34  | 1413 ± 33                                    |
| C100Ph-1<br>$\rho_i = 98$<br>NBS-4<br>D = 433.3   | 1,0                      | 3.893 x 10 <sup>13</sup> | 110.3   | 113.8   | 3.893 x 10 <sup>13</sup> | 1454   | 1409   |
|   | 0,0                      | 3.854 x 10 <sup>13</sup> | 107.0   | 110.4   | 3.854 x 10 <sup>13</sup> | 1514   | 1467   |
|   | -1,0                     | 3.933 x 10 <sup>13</sup> | 111.2   | 114.8   | 3.933 x 10 <sup>13</sup> | 1427   | 1382   |
|   | -1,1                     | 3.555 x 10 <sup>13</sup> | 116.1   | 119.8   | 3.555 x 10 <sup>13</sup> | 1512   | 1466   |
|   | 0,1                      | 3.963 x 10 <sup>13</sup> | 114.4   | 118.0   | 3.963 x 10 <sup>13</sup> | 1377   | 1335   |
|   | 1,1                      | 4.015 x 10 <sup>13</sup> | 109.7   | 113.2   | 4.015 x 10 <sup>13</sup> | 1417   | 1373   |
|   | Avg.                     | 3.869 x 10 <sup>13</sup> | 111.4   | 115.0   | 3.869 x 10 <sup>13</sup> | 1450 ± 55  | 1405 ± 53                                    |
| G65Ph-1<br>$\rho_i = 67.4$<br>NBS-4<br>D = 433.3  | 0,0                      | 6.201 x 10 <sup>13</sup> | 68.07   | 70.25   | 6.201 x 10 <sup>13</sup> | 1479   | 1433   |
|   | -1,0                     | 6.147 x 10 <sup>13</sup> | 69.50   | 71.72   | 6.147 x 10 <sup>13</sup> | 1461   | 1416   |
|   | -1,1                     | 5.892 x 10 <sup>13</sup> | 69.70   | 71.93   | 5.892 x 10 <sup>13</sup> | 1520   | 1473   |
|   | 0,1                      | 6.141 x 10 <sup>13</sup> | 69.92   | 72.15   | 6.141 x 10 <sup>13</sup> | 1454   | 1409   |
|   | 1,1                      | 6.358 x 10 <sup>13</sup> | 69.26   | 71.47   | 6.358 x 10 <sup>13</sup> | 1417   | 1374   |
|   | 1,0                      | 6.127 x 10 <sup>13</sup> | 69.70   | 71.93   | 6.127 x 10 <sup>13</sup> | 1462   | 1416   |
|   | 2,0                      | 6.007 x 10 <sup>13</sup> | 69.60   | 71.82   | 6.007 x 10 <sup>13</sup> | 1493   | 1447   |
| Avg.  | 6.125 x 10 <sup>13</sup> | 69.39                    | 71.61   | 6.125 x 10 <sup>13</sup>                        | 1469 ± 32                | 1424 ± 31  |  |
| C30Ph-1<br>$\rho_i = 31.9$<br>NBS-4<br>D = 433.3  | 1,0                      | 1.149 x 10 <sup>14</sup> | 37.42   | 38.62   | 1.149 x 10 <sup>14</sup> | 1452   | 1407   |
|   | 0,0                      | 1.150 x 10 <sup>14</sup> | 37.29   | 38.48   | 1.150 x 10 <sup>14</sup> | 1455   | 1410   |
|   | -1,0                     | 1.114 x 10 <sup>14</sup> | 37.30   | 38.49   | 1.114 x 10 <sup>14</sup> | 1502   | 1456   |
|   | -1,1                     | 1.126 x 10 <sup>14</sup> | 37.33   | 38.52   | 1.126 x 10 <sup>14</sup> | 1485   | 1439   |
|   | 0,1                      | 1.155 x 10 <sup>14</sup> | 37.35   | 38.54   | 1.155 x 10 <sup>14</sup> | 1447   | 1402   |
|   | 1,1                      | 1.153 x 10 <sup>14</sup> | 37.46   | 38.66   | 1.153 x 10 <sup>14</sup> | 1445   | 1400   |
|   | Avg.                     | 1.141 x 10 <sup>14</sup> | 37.36   | 38.55   | 1.141 x 10 <sup>14</sup> | 1464 ± 23  | 1419 ± 23                                    |
| B12Ph-1<br>$\rho_i = 11.8$<br>NBS-3<br>D = 433.8  | -1,0                     | 3.557 x 10 <sup>14</sup> | 13.15   | 13.57   | 3.557 x 10 <sup>14</sup> | 1334   | 1293   |
|   | -1,1                     | 3.248 x 10 <sup>14</sup> | 12.65   | 13.06   | 3.248 x 10 <sup>14</sup> | 1519   | 1471   |
|   | 0,1                      | 3.623 x 10 <sup>14</sup> | 12.82   | 13.23   | 3.623 x 10 <sup>14</sup> | 1344   | 1302   |
|   | 1,1                      | 3.174 x 10 <sup>14</sup> | 13.29   | 13.72   | 3.174 x 10 <sup>14</sup> | 1480   | 1433   |
|   | -1,2                     | 3.253 x 10 <sup>14</sup> | 13.34   | 13.77   | 3.253 x 10 <sup>14</sup> | 1438   | 1393   |
|   | 0,2                      | 3.363 x 10 <sup>14</sup> | 13.37   | 13.80   | 3.363 x 10 <sup>14</sup> | 1388   | 1345   |
|   | 1,2                      | 3.102 x 10 <sup>14</sup> | 12.91   | 13.33   | 3.102 x 10 <sup>14</sup> | 1559   | 1509   |
|   | -2,1                     | 3.429 x 10 <sup>14</sup> | 12.62   | 13.03   | 3.429 x 10 <sup>14</sup> | 1442   | 1397   |
|   | -2,-1                    | 3.206 x 10 <sup>14</sup> | 13.24   | 13.67   | 3.206 x 10 <sup>14</sup> | 1470   | 1424   |
|   | 1,-1                     | 3.241 x 10 <sup>14</sup> | 12.87   | 13.29   | 3.241 x 10 <sup>14</sup> | 1496   | 1449   |
|   | Avg.                     | 3.320 x 10 <sup>14</sup> | 13.03   | 13.45   | 3.320 x 10 <sup>14</sup> | 1447 ± 74  | 1402 ± 71                                    |
| D9.5Ph-1<br>$\rho_i = 9.51$<br>NBS-3<br>D = 433.1 | 1,0                      | 4.025 x 10 <sup>14</sup> | 10.01   | 10.34   | 4.025 x 10 <sup>14</sup> | 1549   | 1500   |
|   | 0,0                      | 4.552 x 10 <sup>14</sup> | 10.03   | 10.36   | 4.552 x 10 <sup>14</sup> | 1367   | 1324   |
|   | 0,1                      | 4.234 x 10 <sup>14</sup> | 10.58   | 10.92   | 4.234 x 10 <sup>14</sup> | 1393   | 1350   |
|   | -1,1                     | 4.540 x 10 <sup>14</sup> | 10.23   | 10.56   | 4.540 x 10 <sup>14</sup> | 1344   | 1302   |
|   | -1,0                     | 4.297 x 10 <sup>14</sup> | 9.94  | 10.26   | 4.297 x 10 <sup>14</sup> | 1461   | 1416   |
|   | 1,-1                     | 4.339 x 10 <sup>14</sup> | 10.04   | 10.37   | 4.339 x 10 <sup>14</sup> | 1433   | 1387   |
|   | Avg.                     | 4.331 x 10 <sup>14</sup> | 10.14   | 10.47   | 4.331 x 10 <sup>14</sup> | 1425 ± 74  | 1380 ± 72                                    |



Table 1 - Continued

| Wafer Identification                               | Site                     | N<br>cm <sup>-3</sup>    | $\rho_{23^\circ\text{C}}$<br>$\Omega\cdot\text{cm}$ | $\rho_{300\text{ K}}$<br>$\Omega\cdot\text{cm}$ | n<br>cm <sup>-3</sup>    | $\mu_{23^\circ\text{C}}$<br>cm <sup>2</sup> /V·s | $\mu_{300\text{ K}}$<br>cm <sup>2</sup> /V·s |
|--|--------------------------|--------------------------|---|---|--------------------------|--|--|
| F9.1Ph-1<br>$\rho_i = 9.1$<br>NBS-4<br>D = 433.3   | 0,0                      | 4.814 x 10 <sup>14</sup> | 9.107   | 9.391   | 4.814 x 10 <sup>14</sup> | 1424   | 1381   |
|  | -1,0                     | 4.745 x 10 <sup>14</sup> | 9.203   | 9.490   | 4.745 x 10 <sup>14</sup> | 1429   | 1386   |
|  | 0,1                      | 4.723 x 10 <sup>14</sup> | 9.283   | 9.572   | 4.723 x 10 <sup>14</sup> | 1424   | 1381   |
|  | 1,1                      | 4.732 x 10 <sup>14</sup> | 9.208   | 9.496   | 4.732 x 10 <sup>14</sup> | 1432   | 1389   |
|  | 1,0                      | 4.800 x 10 <sup>14</sup> | 9.225   | 9.513   | 4.800 x 10 <sup>14</sup> | 1410   | 1367   |
|  | -2,1                     | 4.802 x 10 <sup>14</sup> | 9.079   | 9.363   | 4.802 x 10 <sup>14</sup> | 1432   | 1388   |
|  | Avg.                     | 4.769 x 10 <sup>14</sup> | 9.184   | 9.471   | 4.769 x 10 <sup>14</sup> | 1425 ± 8   | 1382 ± 8                                     |
| B5.9Ph-1<br>$\rho_i = 5.94$<br>NBS-4<br>D = 433.3  | 0,0                      | 7.646 x 10 <sup>14</sup> | 5.699   | 5.875   | 7.646 x 10 <sup>14</sup> | 1432   | 1389   |
|  | -1,0                     | 7.158 x 10 <sup>14</sup> | 6.481   | 6.681   | 7.158 x 10 <sup>14</sup> | 1345   | 1305   |
|  | -1,1                     | 7.363 x 10 <sup>14</sup> | 6.116   | 6.304   | 7.363 x 10 <sup>14</sup> | 1386   | 1345   |
|  | 0,1                      | 7.272 x 10 <sup>14</sup> | 5.940   | 6.123   | 7.272 x 10 <sup>14</sup> | 1445   | 1402   |
|  | 1,1                      | 7.167 x 10 <sup>14</sup> | 6.327   | 6.522   | 7.167 x 10 <sup>14</sup> | 1376   | 1335   |
|  | 1,0                      | 6.297 x 10 <sup>14</sup> | 6.468   | 6.667   | 6.297 x 10 <sup>14</sup> | 1532   | 1487   |
|  | Avg.                     | 7.150 x 10 <sup>14</sup> | 6.172   | 6.362   | 7.150 x 10 <sup>14</sup> | 1419 ± 66  | 1377 ± 65                                    |
| D2.4Ph-1<br>$\rho_i = 2.35$<br>NBS-3<br>D = 433.1  | -1,1                     | 1.946 x 10 <sup>15</sup> | 2.353   | 2.426   | 1.946 x 10 <sup>15</sup> | 1363   | 1322   |
|  | 0,1                      | 1.968 x 10 <sup>15</sup> | 2.275   | 2.346   | 1.968 x 10 <sup>15</sup> | 1394   | 1352   |
|  | 1,1                      | 2.058 x 10 <sup>15</sup> | 2.352   | 2.425   | 2.058 x 10 <sup>15</sup> | 1289   | 1250   |
|  | -1,0                     | 1.966 x 10 <sup>15</sup> | 2.372   | 2.446   | 1.966 x 10 <sup>15</sup> | 1338   | 1298   |
|  | 0,0                      | 1.842 x 10 <sup>15</sup> | 2.429   | 2.504   | 1.842 x 10 <sup>15</sup> | 1395   | 1354   |
|  | 1,0                      | 1.941 x 10 <sup>15</sup> | 2.405   | 2.480   | 1.941 x 10 <sup>15</sup> | 1337   | 1297   |
|  | -1,-1                    | 1.878 x 10 <sup>15</sup> | 2.432   | 2.508   | 1.878 x 10 <sup>15</sup> | 1367   | 1325   |
|  | 0,-1                     | 1.874 x 10 <sup>15</sup> | 2.455   | 2.531   | 1.874 x 10 <sup>15</sup> | 1357   | 1316   |
|  | Avg.                     | 1.934 x 10 <sup>15</sup> | 2.384   | 2.458   | 1.934 x 10 <sup>15</sup> | 1355 ± 34  | 1314 ± 33                                    |
| B2.1Ph-2<br>$\rho_i = 2.14$<br>NBS-4<br>D = 433.3  | 0,0                      | 2.185 x 10 <sup>15</sup> | 2.129   | 2.192   | 2.185 x 10 <sup>15</sup> | 1342   | 1303   |
|  | 1,0                      | 2.321 x 10 <sup>15</sup> | 1.994   | 2.053   | 2.321 x 10 <sup>15</sup> | 1349   | 1310   |
|  | 1,1                      | 2.368 x 10 <sup>15</sup> | 1.976   | 2.035   | 2.368 x 10 <sup>15</sup> | 1334   | 1295   |
|  | 0,1                      | 2.281 x 10 <sup>15</sup> | 2.003   | 2.062   | 2.281 x 10 <sup>15</sup> | 1366   | 1327   |
|  | -1,1                     | 2.438 x 10 <sup>15</sup> | 1.950   | 2.008   | 2.438 x 10 <sup>15</sup> | 1313   | 1275   |
|  | -1,0                     | 2.389 x 10 <sup>15</sup> | 1.978   | 2.037   | 2.389 x 10 <sup>15</sup> | 1321   | 1283   |
|  | Avg.                     | 2.330 x 10 <sup>15</sup> | 2.005   | 2.064   | 2.330 x 10 <sup>15</sup> | 1338 ± 19  | 1299 ± 19                                    |
| B1.4Ph-3<br>$\rho_i = 1.29$<br>NBS-3<br>D = 433.1  | -1,1                     | 3.749 x 10 <sup>15</sup> | 1.358   | 1.398   | 3.749 x 10 <sup>15</sup> | 1226   | 1191   |
|  | 0,1                      | 3.707 x 10 <sup>15</sup> | 1.314   | 1.353   | 3.707 x 10 <sup>15</sup> | 1281   | 1244   |
|  | 1,1                      | 3.404 x 10 <sup>15</sup> | 1.301   | 1.340   | 3.404 x 10 <sup>15</sup> | 1409   | 1368   |
|  | -1,0                     | 3.460 x 10 <sup>15</sup> | 1.297   | 1.335   | 3.460 x 10 <sup>15</sup> | 1391   | 1351   |
|  | 0,0                      | 3.859 x 10 <sup>15</sup> | 1.253   | 1.290   | 3.859 x 10 <sup>15</sup> | 1291   | 1254   |
|  | 1,0                      | 3.278 x 10 <sup>15</sup> | 1.296   | 1.334   | 3.278 x 10 <sup>15</sup> | 1469   | 1427   |
|  | 0,-1                     | 3.553 x 10 <sup>15</sup> | 1.392   | 1.433   | 3.553 x 10 <sup>15</sup> | 1262   | 1226   |
| Avg.   | 3.573 x 10 <sup>15</sup> | 1.316                    | 1.355   | 3.573 x 10 <sup>15</sup>                        | 1332 ± 90                | 1295 ± 87  |  |
| A1.0Ph-1<br>$\rho_i = 1.01$<br>NBS-3<br>D = 432.8  | 0,-1                     | 4.800 x 10 <sup>15</sup> | 1.019   | 1.049   | 4.800 x 10 <sup>15</sup> | 1276   | 1240   |
|  | -1,0                     | 4.885 x 10 <sup>15</sup> | 1.005   | 1.034   | 4.885 x 10 <sup>15</sup> | 1271   | 1236   |
|  | -1,1                     | 4.596 x 10 <sup>15</sup> | 1.024   | 1.054   | 4.596 x 10 <sup>15</sup> | 1326   | 1288   |
|  | -2,1                     | 4.675 x 10 <sup>15</sup> | 1.040   | 1.071   | 4.675 x 10 <sup>15</sup> | 1284   | 1247   |
|  | Avg.                     | 4.739 x 10 <sup>15</sup> | 1.022   | 1.052   | 4.739 x 10 <sup>15</sup> | 1289 ± 25  | 1253 ± 24                                    |
| B0.80Ph-1<br>$\rho_i = 0.79$<br>NBS-4<br>D = 433.3 | 1,0                      | 6.098 x 10 <sup>15</sup> | 0.7887  | 0.8106  | 6.098 x 10 <sup>15</sup> | 1298   | 1263   |
|  | 0,0                      | 6.716 x 10 <sup>15</sup> | 0.7643  | 0.7855  | 6.716 x 10 <sup>15</sup> | 1216   | 1183   |
|  | 1,1                      | 6.353 x 10 <sup>15</sup> | 0.7834  | 0.8051  | 6.353 x 10 <sup>15</sup> | 1254   | 1220   |
|  | 0,1                      | 5.920 x 10 <sup>15</sup> | 0.8122  | 0.8347  | 5.920 x 10 <sup>15</sup> | 1298   | 1263   |
|  | -1,1                     | 5.958 x 10 <sup>15</sup> | 0.8067  | 0.8291  | 5.958 x 10 <sup>15</sup> | 1299   | 1264   |
|  | -1,0                     | 6.211 x 10 <sup>15</sup> | 0.7807  | 0.8023  | 6.211 x 10 <sup>15</sup> | 1287   | 1253   |
|  | Avg.                     | 6.210 x 10 <sup>15</sup> | 0.7893  | 0.8112  | 6.210 x 10 <sup>15</sup> | 1275 ± 34  | 1241 ± 33                                    |

Table 1 - Continued

| Wafer Identification                                | Site                     | N<br>cm <sup>-3</sup>    | $\rho_{23^\circ\text{C}}$<br>$\Omega \cdot \text{cm}$ | $\rho_{300\text{ K}}$<br>$\Omega \cdot \text{cm}$ | n<br>cm <sup>-3</sup>    | $\mu_{23^\circ\text{C}}$<br>cm <sup>2</sup> /V·s | $\mu_{300\text{ K}}$<br>cm <sup>2</sup> /V·s |
|---|--------------------------|--------------------------|---|---|--------------------------|--|--|
| B0.77Ph-1<br>$\rho_i = 0.77$<br>NBS-3<br>D = 433.1  | 0,1                      | 6.251 x 10 <sup>15</sup> | 0.7912  | 0.8138  | 6.251 x 10 <sup>15</sup> | 1262   | 1227   |
|   | 1,1                      | 6.400 x 10 <sup>15</sup> | 0.7771  | 0.7993  | 6.400 x 10 <sup>15</sup> | 1255   | 1220   |
|   | -1,0                     | 6.630 x 10 <sup>15</sup> | 0.7656  | 0.7874  | 6.630 x 10 <sup>15</sup> | 1230   | 1196   |
|   | 0,0                      | 6.673 x 10 <sup>15</sup> | 0.7647  | 0.7865  | 6.673 x 10 <sup>15</sup> | 1223   | 1189   |
|   | 1,0                      | 6.257 x 10 <sup>15</sup> | 0.7731  | 0.7951  | 6.257 x 10 <sup>15</sup> | 1290   | 1255   |
|   | 0,-1                     | 5.955 x 10 <sup>15</sup> | 0.7990  | 0.8218  | 5.955 x 10 <sup>15</sup> | 1312   | 1275   |
|   | Avg.                     | 6.361 x 10 <sup>15</sup> | 0.7785  | 0.8007  | 6.361 x 10 <sup>15</sup> | 1262 ± 34  | 1227 ± 33                                    |
| B0.47Ph-1<br>$\rho_i = 0.47$<br>NBS-3<br>D = 432.8  | 0,0                      | 1.132 x 10 <sup>16</sup> | 0.4834  | 0.4964  | 1.131 x 10 <sup>16</sup> | 1142   | 1112   |
|   | 0,1                      | 1.175 x 10 <sup>16</sup> | 0.4856  | 0.4987  | 1.174 x 10 <sup>16</sup> | 1095   | 1066   |
|   | -1,0                     | 1.122 x 10 <sup>16</sup> | 0.4778  | 0.4907  | 1.121 x 10 <sup>16</sup> | 1165   | 1135   |
|   | -1,1                     | 1.072 x 10 <sup>16</sup> | 0.4912  | 0.5044  | 1.071 x 10 <sup>16</sup> | 1186   | 1155   |
|   | -2,1                     | 0.974 x 10 <sup>16</sup> | 0.5027  | 0.5162  | 0.973 x 10 <sup>16</sup> | 1276   | 1243   |
|   | -2,0                     | 1.027 x 10 <sup>16</sup> | 0.5133  | 0.5271  | 1.026 x 10 <sup>16</sup> | 1185   | 1154   |
|   | -1,-1                    | 1.115 x 10 <sup>16</sup> | 0.4735  | 0.4862  | 1.114 x 10 <sup>16</sup> | 1183   | 1152   |
|   | 1,0                      | 1.032 x 10 <sup>16</sup> | 0.4965  | 0.5099  | 1.031 x 10 <sup>16</sup> | 1219   | 1187   |
| Avg.  | 1.081 x 10 <sup>16</sup> | 0.4905                   | 0.5037  | 1.080 x 10 <sup>16</sup>                          | 1181 ± 53                | 1150 ± 52  |  |
| B0.40Ph-1<br>$\rho_i = 0.40$<br>NBS-4<br>D = 433.3  | -1,-1                    | 1.485 x 10 <sup>16</sup> | 0.3586  | 0.3677  | 1.484 x 10 <sup>16</sup> | 1173   | 1144   |
|   | 0,0                      | 1.145 x 10 <sup>16</sup> | 0.4442  | 0.4555  | 1.144 x 10 <sup>16</sup> | 1228   | 1198   |
|   | -1,0                     | 1.303 x 10 <sup>16</sup> | 0.4201  | 0.4308  | 1.302 x 10 <sup>16</sup> | 1141   | 1270   |
|   | -1,1                     | 1.226 x 10 <sup>16</sup> | 0.4545  | 0.4660  | 1.225 x 10 <sup>16</sup> | 1121   | 1093   |
|   | 0,1                      | 1.186 x 10 <sup>16</sup> | 0.4542  | 0.4657  | 1.185 x 10 <sup>16</sup> | 1160   | 1131   |
|   | 1,1                      | 1.807 x 10 <sup>16</sup> | 0.3280  | 0.3363  | 1.806 x 10 <sup>16</sup> | 1054   | 1028   |
|   | 1,0                      | 1.603 x 10 <sup>16</sup> | 0.3605  | 0.3697  | 1.602 x 10 <sup>16</sup> | 1081   | 1054   |
|   | 0,-1                     | 1.198 x 10 <sup>16</sup> | 0.4115  | 0.4220  | 1.197 x 10 <sup>16</sup> | 1267   | 1236   |
|   | 1,-1                     | 1.624 x 10 <sup>16</sup> | 0.3532  | 0.3622  | 1.623 x 10 <sup>16</sup> | 1089   | 1062   |
|   | Avg.                     | 1.397 x 10 <sup>16</sup> | 0.3983  | 0.4084  | 1.396 x 10 <sup>16</sup> | 1146 ± 70  | 1101 ± 75                                    |
| B0.30Ph-1<br>$\rho_i = 0.285$<br>NBS-4<br>D = 433.3 | 0,0                      | 2.004 x 10 <sup>16</sup> | 0.2845  | 0.2915  | 2.000 x 10 <sup>16</sup> | 1097   | 1071   |
|   | 1,0                      | 1.945 x 10 <sup>16</sup> | 0.2869  | 0.2940  | 1.941 x 10 <sup>16</sup> | 1121   | 1094   |
|   | 1,1                      | 2.110 x 10 <sup>16</sup> | 0.2782  | 0.2851  | 2.106 x 10 <sup>16</sup> | 1065   | 1040   |
|   | 0,1                      | 2.025 x 10 <sup>16</sup> | 0.2899  | 0.2970  | 2.021 x 10 <sup>16</sup> | 1065   | 1040   |
|   | -1,1                     | 2.070 x 10 <sup>16</sup> | 0.2828  | 0.2898  | 2.066 x 10 <sup>16</sup> | 1068   | 1042   |
|   | -1,0                     | 2.046 x 10 <sup>16</sup> | 0.2872  | 0.2943  | 2.042 x 10 <sup>16</sup> | 1064   | 1039   |
| Avg.  | 2.033 x 10 <sup>16</sup> | 0.2849                   | 0.2920  | 2.029 x 10 <sup>16</sup>                          | 1080 ± 24                | 1054 ± 23  |  |
| A0.27Ph-2<br>$\rho_i = 0.269$<br>NBS-3<br>D = 432.8 | 0,0                      | 2.171 x 10 <sup>16</sup> | 0.2748  | 0.2815  | 2.165 x 10 <sup>16</sup> | 1049   | 1024   |
|   | 0,1                      | 2.093 x 10 <sup>16</sup> | 0.2708  | 0.2774  | 2.087 x 10 <sup>16</sup> | 1104   | 1078   |
|   | -1,0                     | 2.094 x 10 <sup>16</sup> | 0.2673  | 0.2738  | 2.088 x 10 <sup>16</sup> | 1118   | 1092   |
|   | -1,1                     | 2.090 x 10 <sup>16</sup> | 0.2746  | 0.2813  | 2.084 x 10 <sup>16</sup> | 1091   | 1065   |
|   | Avg.                     | 2.112 x 10 <sup>16</sup> | 0.2719  | 0.2785  | 2.106 x 10 <sup>16</sup> | 1090 ± 30  | 1065 ± 29                                    |
| B0.18Ph-2<br>$\rho_i = 0.192$<br>NBS-4<br>D = 433.3 | 0,0                      | 3.308 x 10 <sup>16</sup> | 0.1900  | 0.1943  | 3.288 x 10 <sup>16</sup> | 999  | 977  |
|   | -1,0                     | 3.342 x 10 <sup>16</sup> | 0.1927  | 0.1970  | 3.322 x 10 <sup>16</sup> | 975  | 954  |
|   | -1,1                     | 3.267 x 10 <sup>16</sup> | 0.1924  | 0.1967  | 3.247 x 10 <sup>16</sup> | 999  | 977  |
|   | 0,1                      | 3.177 x 10 <sup>16</sup> | 0.1980  | 0.2024  | 3.158 x 10 <sup>16</sup> | 998  | 976  |
|   | 1,1                      | 3.356 x 10 <sup>16</sup> | 0.1911  | 0.1953  | 3.336 x 10 <sup>16</sup> | 979  | 958  |
|   | 1,0                      | 3.235 x 10 <sup>16</sup> | 0.1953  | 0.1997  | 3.215 x 10 <sup>16</sup> | 994  | 972  |
| Avg.  | 3.281 x 10 <sup>16</sup> | 0.1932                   | 0.1976  | 3.261 x 10 <sup>16</sup>                          | 991 ± 11                 | 969 ± 10   |  |
| B0.12Ph-1<br>$\rho_i = 0.124$<br>NBS-4<br>D = 433.3 | -1,0                     | 5.730 x 10 <sup>16</sup> | 0.1225  | 0.1250  | 5.667 x 10 <sup>16</sup> | 899  | 881  |
|   | 0,0                      | 5.514 x 10 <sup>16</sup> | 0.1221  | 0.1245  | 5.453 x 10 <sup>16</sup> | 937  | 919  |
|   | 1,0                      | 6.691 x 10 <sup>16</sup> | 0.1249  | 0.1274  | 6.617 x 10 <sup>16</sup> | 755  | 740  |
|   | -1,1                     | 5.667 x 10 <sup>16</sup> | 0.1070  | 0.1091  | 5.604 x 10 <sup>16</sup> | 1041   | 1021   |
|   | 0,1                      | 5.840 x 10 <sup>16</sup> | 0.1289  | 0.1315  | 5.776 x 10 <sup>16</sup> | 838  | 822  |
|   | 1,1                      | 5.041 x 10 <sup>16</sup> | 0.1235  | 0.1260  | 4.985 x 10 <sup>16</sup> | 1014   | 994  |
|   | -1,-1                    | 5.981 x 10 <sup>16</sup> | 0.1152  | 0.1175  | 5.915 x 10 <sup>16</sup> | 916  | 898  |
|   | 1,-1                     | 5.932 x 10 <sup>16</sup> | 0.1296  | 0.1322  | 5.867 x 10 <sup>16</sup> | 821  | 805  |
| Avg.  | 5.800 x 10 <sup>16</sup> | 0.1217                   | 0.1242  | 5.736 x 10 <sup>16</sup>                          | 903 ± 97                 | 885 ± 95   |  |

Table 1 - Continued

| Wafer Identification                                 | Site                     | N<br>cm <sup>-3</sup>    | $\rho_{23^\circ\text{C}}$<br>$\Omega \cdot \text{cm}$ | $\rho_{300\text{ K}}$<br>$\Omega \cdot \text{cm}$ | n<br>cm <sup>-3</sup>    | $\mu_{23^\circ\text{C}}$<br>cm <sup>2</sup> /V·s | $\mu_{300\text{ K}}$<br>cm <sup>2</sup> /V·s |
|--|--------------------------|--------------------------|---|---|--------------------------|--|--|
| B0.099Ph-3<br>$\rho_i = 0.092$<br>NBS-4<br>D = 433.3 | -1,1                     | 8.965 x 10 <sup>16</sup> | 0.09077   | 0.09238   | 8.831 x 10 <sup>16</sup> | 779  | 765  |
|  | -1,0                     | 9.557 x 10 <sup>16</sup> | 0.08933   | 0.09091   | 9.414 x 10 <sup>16</sup> | 742  | 729  |
|  | 0,0                      | 9.735 x 10 <sup>16</sup> | 0.08695   | 0.08849   | 9.589 x 10 <sup>16</sup> | 749  | 735  |
|  | 1,0                      | 8.766 x 10 <sup>16</sup> | 0.08959   | 0.09118   | 8.635 x 10 <sup>16</sup> | 807  | 793  |
|  | 1,1                      | 9.555 x 10 <sup>16</sup> | 0.09381   | 0.09547   | 9.412 x 10 <sup>16</sup> | 707  | 695  |
|  | 0,1                      | 9.078 x 10 <sup>16</sup> | 0.08953   | 0.09112   | 8.942 x 10 <sup>16</sup> | 780  | 766  |
| Avg.   | 9.276 x 10 <sup>16</sup> | 0.09000                  | 0.09159   | 9.137 x 10 <sup>16</sup>                          | 761 ± 35                 | 747 ± 34   |  |
| B0.080Ph-1<br>$\rho_i = 0.080$<br>NBS-4<br>D = 433.3 | 1,-1                     | 1.131 x 10 <sup>17</sup> | 0.07776   | 0.07905   | 1.109 x 10 <sup>17</sup> | 724  | 712  |
|  | -1,-1                    | 1.090 x 10 <sup>17</sup> | 0.07835   | 0.07965   | 1.069 x 10 <sup>17</sup> | 745  | 733  |
|  | -1,1                     | 1.101 x 10 <sup>17</sup> | 0.07943   | 0.08074   | 1.080 x 10 <sup>17</sup> | 728  | 716  |
|  | 0,1                      | 1.053 x 10 <sup>17</sup> | 0.08100   | 0.08234   | 1.033 x 10 <sup>17</sup> | 746  | 734  |
|  | 1,1                      | 1.165 x 10 <sup>17</sup> | 0.07881   | 0.08011   | 1.143 x 10 <sup>17</sup> | 693  | 682  |
|  | 1,0                      | 1.086 x 10 <sup>17</sup> | 0.08004   | 0.08137   | 1.065 x 10 <sup>17</sup> | 732  | 720  |
|  | 0,0                      | 1.039 x 10 <sup>17</sup> | 0.08058   | 0.08191   | 1.019 x 10 <sup>17</sup> | 760  | 748  |
|  | 0,-1                     | 1.090 x 10 <sup>17</sup> | 0.07891   | 0.08022   | 1.069 x 10 <sup>17</sup> | 740  | 728  |
|  | Avg.                     | 1.094 x 10 <sup>17</sup> | 0.07936   | 0.08067   | 1.073 x 10 <sup>17</sup> | 734 ± 20   | 722 ± 20                                     |
| A0.060Ph-3<br>$\rho_i = 0.062$<br>NBS-4<br>D = 433.3 | -1,0                     | 1.459 x 10 <sup>17</sup> | 0.06375   | 0.06466   | 1.421 x 10 <sup>17</sup> | 689  | 679  |
|  | -1,1                     | 1.544 x 10 <sup>17</sup> | 0.06473   | 0.06565   | 1.504 x 10 <sup>17</sup> | 641  | 632  |
|  | 0,1                      | 1.808 x 10 <sup>17</sup> | 0.05920   | 0.06004   | 1.761 x 10 <sup>17</sup> | 599  | 590  |
|  | 1,1                      | 1.576 x 10 <sup>17</sup> | 0.06189   | 0.06277   | 1.535 x 10 <sup>17</sup> | 657  | 648  |
|  | 1,0                      | 1.566 x 10 <sup>17</sup> | 0.06042   | 0.06128   | 1.525 x 10 <sup>17</sup> | 677  | 668  |
|  | 0,0                      | 1.913 x 10 <sup>17</sup> | 0.05820   | 0.05903   | 1.863 x 10 <sup>17</sup> | 576  | 568  |
| Avg.   | 1.644 x 10 <sup>17</sup> | 0.06137                  | 0.06224   | 1.601 x 10 <sup>17</sup>                          | 640 ± 44                 | 631 ± 44   |  |
| B0.050Ph-3<br>$\rho_i = 0.051$<br>NBS-4<br>D = 433.3 | 1,2                      | 2.234 x 10 <sup>17</sup> | 0.05285   | 0.05350   | 2.160 x 10 <sup>17</sup> | 547  | 540  |
|  | 0,2                      | 2.145 x 10 <sup>17</sup> | 0.05115   | 0.05178   | 2.074 x 10 <sup>17</sup> | 588  | 581  |
|  | 1,3                      | 2.135 x 10 <sup>17</sup> | 0.05439   | 0.05506   | 2.064 x 10 <sup>17</sup> | 556  | 549  |
|  | 0,3                      | 2.114 x 10 <sup>17</sup> | 0.05334   | 0.05400   | 2.044 x 10 <sup>17</sup> | 572  | 566  |
|  | -1,3                     | 2.070 x 10 <sup>17</sup> | 0.05453   | 0.05520   | 2.001 x 10 <sup>17</sup> | 572  | 565  |
| Avg.   | 2.140 x 10 <sup>17</sup> | 0.05325                  | 0.05391   | 2.069 x 10 <sup>17</sup>                          | 567 ± 16                 | 560 ± 16   |  |
| B0.034Ph-1<br>$\rho_i = 0.034$<br>NBS-4<br>D = 433.3 | -1,0                     | 5.112 x 10 <sup>17</sup> | 0.03410   | 0.03438   | 4.811 x 10 <sup>17</sup> | 380  | 377  |
|  | -1,1                     | 4.764 x 10 <sup>17</sup> | 0.03481   | 0.03509   | 4.483 x 10 <sup>17</sup> | 400  | 397  |
|  | 0,1                      | 4.284 x 10 <sup>17</sup> | 0.03527   | 0.03556   | 4.031 x 10 <sup>17</sup> | 439  | 435  |
|  | 1,1                      | 4.782 x 10 <sup>17</sup> | 0.03422   | 0.03450   | 4.500 x 10 <sup>17</sup> | 405  | 402  |
|  | 1,0                      | 5.081 x 10 <sup>17</sup> | 0.03434   | 0.03462   | 4.781 x 10 <sup>17</sup> | 380  | 377  |
|  | 0,0                      | 5.386 x 10 <sup>17</sup> | 0.03508   | 0.03536   | 5.068 x 10 <sup>17</sup> | 351  | 348  |
| Avg.   | 4.901 x 10 <sup>17</sup> | 0.03464                  | 0.03492   | 4.612 x 10 <sup>17</sup>                          | 392 ± 30                 | 389 ± 29   |  |
| B0.031Ph-1<br>$\rho_i = 0.032$<br>NBS-4<br>D = 433.1 | -1,1                     | 5.085 x 10 <sup>17</sup> | 0.03152   | 0.03172   | 4.775 x 10 <sup>17</sup> | 415  | 412  |
|  | 0,1                      | 5.067 x 10 <sup>17</sup> | 0.03200   | 0.03220   | 4.758 x 10 <sup>17</sup> | 410  | 407  |
|  | 1,1                      | 5.290 x 10 <sup>17</sup> | 0.03149   | 0.03169   | 4.967 x 10 <sup>17</sup> | 399  | 396  |
|  | -1,0                     | 5.437 x 10 <sup>17</sup> | 0.03157   | 0.03177   | 5.105 x 10 <sup>17</sup> | 387  | 385  |
|  | 0,0                      | 5.740 x 10 <sup>17</sup> | 0.02991   | 0.03010   | 5.390 x 10 <sup>17</sup> | 387  | 385  |
|  | 1,0                      | 4.827 x 10 <sup>17</sup> | 0.03297   | 0.03318   | 4.532 x 10 <sup>17</sup> | 418  | 415  |
| Avg.   | 5.241 x 10 <sup>17</sup> | 0.03158                  | 0.03178   | 4.921 x 10 <sup>17</sup>                          | 403 ± 14                 | 400 ± 13   |  |

calculated from the dopant density using the results of Li and Thurber [30] for the fraction of dopant which is ionized. Columns 7 and 8 give the electron mobility,  $\mu$ , calculated for temperatures of both 23°C and 300 K, respectively, using the relationship  $\mu = 1/qn\rho$  where  $q$  is the electronic charge,  $n$  is the electron density, and  $\rho$  is the resistivity.

Table 2 gives the Hall coefficient, electron density, resistivity, and mobility for the phosphorus-doped silicon van der Pauw specimens measured at both 23°C and 300 K. A comparison of the Hall coefficient results at the two temperatures gives a measure of the experimental reproducibility as the Hall coefficient at 23°C should be essentially the same as that at 300 K. The results are usually within 0.2 percent, and the largest discrepancy is 0.5 percent. In all cases the resistivity at 300 K is larger than at 23°C as expected from the positive temperature coefficient of resistivity [20].

In addition to the C-V and Hall effect work discussed in this report, neutron activation analysis and photometric measurements of total phosphorus density were made outside NBS on material used in this study. These techniques and a comparison of the results obtained from them are discussed in detail elsewhere [31]. A complete listing of data for slices analyzed by neutron activation analysis is given in table 3. Data for slices analyzed by the photometric technique are given in table 4.

Figure 4 shows the product of resistivity and dopant density as a function of resistivity at 300 K. Since, to a first approximation, resistivity is inversely proportional to dopant density, a plot of the product allows deviations from this inverse relationship to be more easily seen, particularly for low resistivities where the product is large. As seen in figure 4, there is a systematic difference between the results from neutron activation analysis and those from the photometric technique. The data points from the Hall effect, which measures only electrically active phosphorus, lie between the two nonelectrical techniques. Neutron activation analysis and C-V agree within experimental error for phosphorus densities in the range of  $10^{16}$  to  $5 \times 10^{17}$   $\text{cm}^{-3}$ . The data of Mousty *et al.* [32], obtained from resistivity measurements and either neutron activation analysis or Hall effect for phosphorus density, are also plotted in figure 4. Their results are in reasonable agreement with this work except at the low resistivity end where differences are as large as 15 percent.

Throughout the resistivity range, the data obtained in the present study are displaced from the Irvin curve [2], also shown in figure 4, in the direction of lower dopant density for a given resistivity. The difference varies between 5 and 15 percent over the resistivity range with somewhat larger deviations below  $1 \Omega \cdot \text{cm}$  than above.

Figure 5 is a graph of electron mobility at 300 K as a function of electron density. The theoretical curve of Li and Thurber [30] is in good agreement with the experimental results. The Caughey and Thomas [1] mobility expression for *n*-type silicon gives significantly lower mobility at low electron density. The Caughey and Thomas expression is a fit to the Irvin curve with the assumption that the electron density equals the dopant density. This is true for lightly doped material ( $<10^{17} \text{ cm}^{-3}$ ), but calculations [30] indicate that the electron density is less than the dopant density for material in the

Table 2. Data for Phosphorus-Doped Silicon Obtained from van der Pauw Specimens.

| Specimen No. | T = 23°C                   |                          |                             |                              | T = 300 K                  |                          |                             |                              |
|--------------|----------------------------|--------------------------|-----------------------------|------------------------------|----------------------------|--------------------------|-----------------------------|------------------------------|
|              | $R_H$ (cm <sup>3</sup> /C) | n (cm <sup>-3</sup> )    | $\rho$ ( $\Omega \cdot$ cm) | $\mu$ (cm <sup>2</sup> /V·s) | $R_H$ (cm <sup>3</sup> /C) | n (cm <sup>-3</sup> )    | $\rho$ ( $\Omega \cdot$ cm) | $\mu$ (cm <sup>2</sup> /V·s) |
| 0.0047Ph-A   | -0.4815                    | 1.296 x 10 <sup>19</sup> | 0.004766                    | 101.0                        | -0.4812                    | 1.297 x 10 <sup>19</sup> | 0.004781                    | 100.6                        |
| 0.0045Ph-39  | -0.4365                    | 1.430 x 10 <sup>19</sup> | 0.004335                    | 100.7                        | -0.4367                    | 1.429 x 10 <sup>19</sup> | 0.004353                    | 100.3                        |
| 0.0033Ph-L31 | -0.3167                    | 1.971 x 10 <sup>19</sup> | 0.003304                    | 95.8                         | -0.3172                    | 1.968 x 10 <sup>19</sup> | 0.003322                    | 95.5                         |
| 0.0026Ph-A   | -0.2150                    | 2.903 x 10 <sup>19</sup> | 0.002327                    | 92.4                         | -0.2146                    | 2.908 x 10 <sup>19</sup> | 0.002345                    | 91.5                         |
| 0.0020Ph-47  | -0.1802                    | 3.464 x 10 <sup>19</sup> | 0.002000                    | 90.1                         | -0.1792                    | 3.483 x 10 <sup>19</sup> | 0.002015                    | 88.9                         |
| 0.0020Ph-19  | -0.1783                    | 3.501 x 10 <sup>19</sup> | 0.001984                    | 89.9                         | -0.1780                    | 3.506 x 10 <sup>19</sup> | 0.001999                    | 89.1                         |
| 0.0017Ph-A   | -0.1431                    | 4.362 x 10 <sup>19</sup> | 0.001597                    | 89.6                         | -0.1430                    | 4.365 x 10 <sup>19</sup> | 0.001611                    | 88.8                         |
| 0.0015Ph-A   | -0.1286                    | 4.853 x 10 <sup>19</sup> | 0.001444                    | 89.1                         | -0.1289                    | 4.842 x 10 <sup>19</sup> | 0.001456                    | 88.5                         |
| 0.0012Ph-A   | -0.1068                    | 5.844 x 10 <sup>19</sup> | 0.001225                    | 87.2                         | -0.1065                    | 5.860 x 10 <sup>19</sup> | 0.001235                    | 86.2                         |
| 0.0013Ph-46  | -0.1047                    | 5.961 x 10 <sup>19</sup> | 0.001200                    | 87.3                         | -0.1046                    | 5.967 x 10 <sup>19</sup> | 0.001210                    | 86.4                         |
| 0.0011Ph-A   | -0.0879                    | 7.101 x 10 <sup>19</sup> | 0.001044                    | 84.2                         | -0.0881                    | 7.084 x 10 <sup>19</sup> | 0.001054                    | 83.6                         |
| 0.0009Ph-A   | -0.0690                    | 9.046 x 10 <sup>19</sup> | 0.000857                    | 80.5                         | -0.0693                    | 9.006 x 10 <sup>19</sup> | 0.000864                    | 80.2                         |

Table 3. Data for Silicon Slices with the Phosphorus Density Determined by Neutron Activation Analysis.

| Slice No. | $\rho_{23^\circ\text{C}}$<br>$\Omega \cdot \text{cm}$ | N<br>$\text{cm}^{-3}$          |
|-----------|---|--------------------------------|
| 46-1      | 0.00129   | $5.85 \pm 0.11 \times 10^{19}$ |
| 47-1      | 0.00201   | $3.66 \pm 0.10 \times 10^{19}$ |
| 39-1      | 0.00448   | $1.54 \pm 0.01 \times 10^{19}$ |
| 26-1      | 0.00697   | $9.10 \pm 0.09 \times 10^{18}$ |
| 52-1      | 0.0101  | $5.25 \pm 0.10 \times 10^{18}$ |
| 52-3      | 0.0105  | $4.93 \pm 0.08 \times 10^{18}$ |
| 25-1      | 0.0340  | $4.51 \pm 0.10 \times 10^{17}$ |
| 48-1      | 0.0520  | $2.28 \pm 0.08 \times 10^{17}$ |
| 48-2      | 0.0531  | $2.12 \pm 0.05 \times 10^{17}$ |
| 34-1      | 0.0785  | $1.20 \pm 0.01 \times 10^{17}$ |
| 34-2      | 0.0759  | $1.19 \pm 0.04 \times 10^{17}$ |
| 51-1      | 0.193   | $3.9 \pm 0.6 \times 10^{16}$   |
| 40-1      | 0.281   | $2.03 \pm 0.13 \times 10^{16}$ |
| 70-1      | 0.404   | $1.50 \pm 0.05 \times 10^{16}$ |
| 70-2      | 0.387   | $1.53 \pm 0.07 \times 10^{16}$ |
| 29-1      | 0.492   | $1.16 \pm 0.08 \times 10^{16}$ |
| 38-1      | 0.805   | $7.35 \pm 0.35 \times 10^{15}$ |
| 49-2      | 1.40  | $4.99 \pm 0.39 \times 10^{15}$ |

Table 4. Data for Silicon Slices with the Phosphorus Density Determined by the Photometric Technique.

| Slice No. | $\rho_{23^\circ\text{C}}$<br>$\Omega \cdot \text{cm}$ | N<br>$\text{cm}^{-3}$ |
|-----------|---|-----------------------|
| 46-2      | 0.00130   | $5.17 \times 10^{19}$ |
| 47-2      | 0.00219   | $3.02 \times 10^{19}$ |
| L31-5     | 0.00378   | $1.65 \times 10^{19}$ |
| 39-2      | 0.00457   | $1.22 \times 10^{19}$ |
| 26-2      | 0.00730   | $7.70 \times 10^{18}$ |
| 52-2      | 0.0101  | $4.44 \times 10^{18}$ |
| 14-A      | 0.0144  | $2.40 \times 10^{18}$ |
| 25-L      | 0.0333  | $4.30 \times 10^{17}$ |
| 48-L      | 0.0501  | $2.27 \times 10^{17}$ |

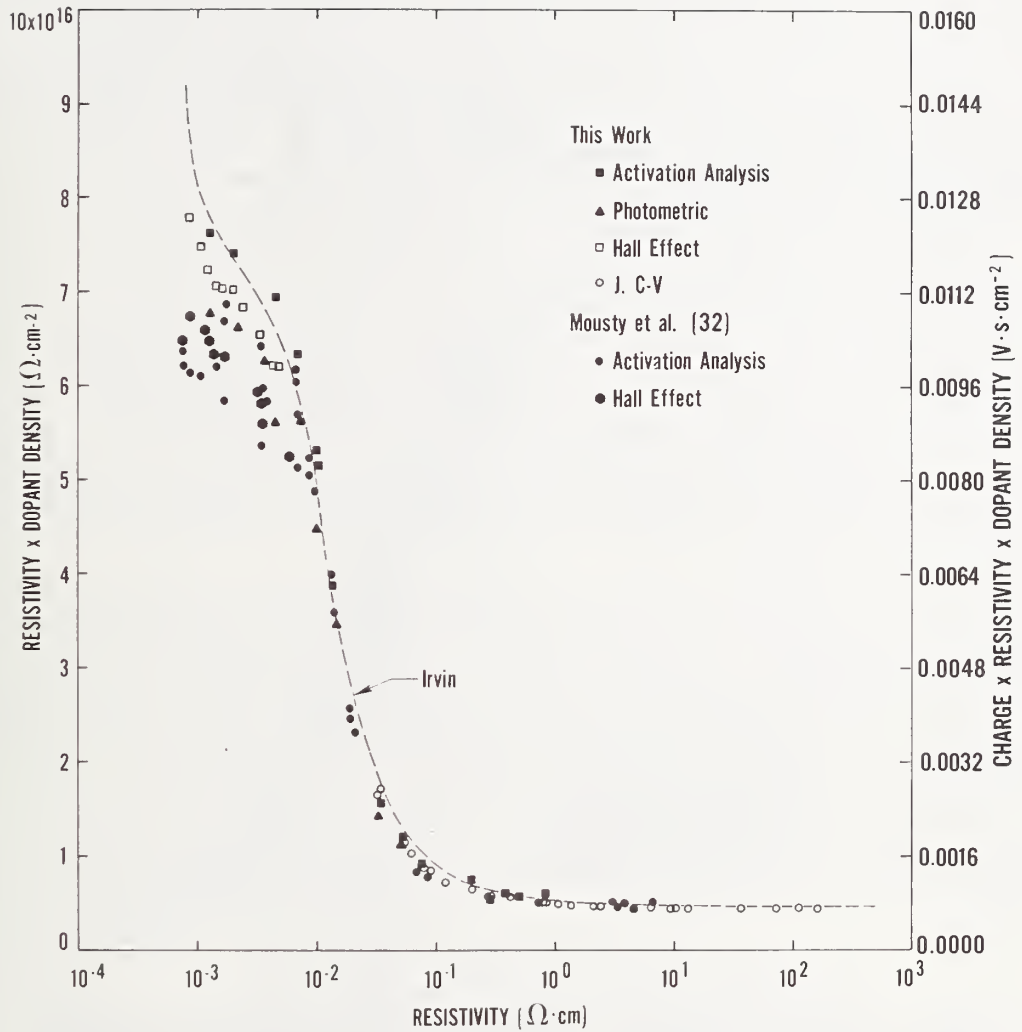


Figure 4. Resistivity-dopant density product for phosphorus-doped silicon at 300 K. Results of this work are compared with those of Mousty *et al.* [32] and Irvin [2]. Values of the  $q\rho N$  product are on the right ordinate.

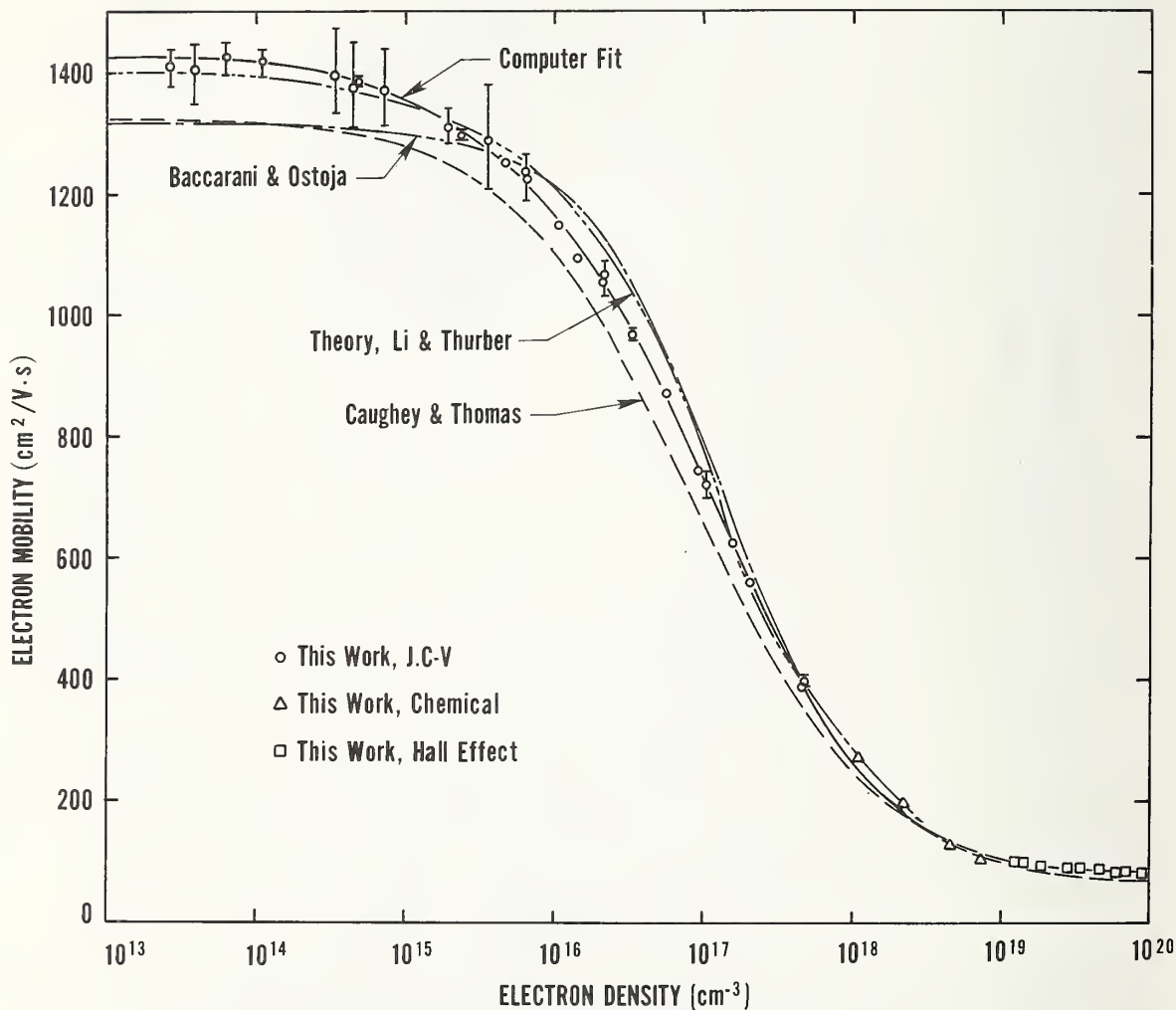


Figure 5. Electron mobility as a function of electron density for phosphorus-doped silicon at 300 K. The junction C-V data have been corrected for deionization using the calculations of Li and Thurber [30]. The error bars are the standard deviation in the individual mobility values for that wafer. When not shown, the error bars lie within the plotted symbol. Shown for comparison with the computer fit to the data are the mobility expressions of Caughey and Thomas [1], Baccarani and Ostoja [3], and the theoretical calculation of Li and Thurber [30].



$10^{17} \text{ cm}^{-3}$  to mid- $10^{18} \text{ cm}^{-3}$  range. In the heavily doped range, the two densities are again equal except for the formation of phosphorus-vacancy pairs, which give rise to electrically inactive atoms, at phosphorus densities greater than about  $5 \times 10^{19} \text{ cm}^{-3}$  [33].

Also shown in figure 5 is the mobility expression of Baccarani and Ostoja [3] based on the data of Mousty *et al.* [32], with the assumption that electron and dopant densities are equal. For comparison with the other curves the Baccarani and Ostoja expression has been corrected to 300 K since the Mousty data were taken at 23°C. At low dopant densities, the Baccarani and Ostoja curve is about 7 percent below the data of this work. In the range  $10^{16}$  to  $5 \times 10^{17} \text{ cm}^{-3}$ , their curve is parallel to, but about 5 percent above, the results of this work. At high dopant densities, the Baccarani and Ostoja curve gives values between 10 and 20 percent larger than those obtained in this work as is seen more clearly in figure 6, which is a detailed expansion of the high density portion of figure 5.

In figure 6, all of the results shown were obtained by Hall effect and resistivity measurements with the assumption that the Hall scattering factor was unity. In this dopant range, the Caughey and Thomas curve is lower and the Baccarani and Ostoja curve is higher than the results of this work. The modification of the Caughey-Thomas expression shown in the figure consists of multiplying the constant  $\mu_{\min}$  in the Caughey-Thomas expression by a term which decreases  $\mu_{\min}$  at high electron densities [34]. The computer fit to the present data (open rectangular points) is also shown in figure 6.

With the exception of the data point of Fair and Tsai [35], all of the results in figure 6 were obtained on silicon doped during crystal growth. Recently, Masetti and Solmi [36] have made extensive measurements on silicon heavily doped by thermal diffusion. Their mobility values obtained from incremental sheet resistance and Hall effect measurements are in good agreement with those of this work. They concluded, from a comparison of their data with those of Mousty *et al.*, that the mobility in diffused phosphorus-doped silicon is always lower than that in uniformly doped silicon for  $n > 10^{19} \text{ cm}^{-3}$ . However, when the results of Masetti and Solmi are compared with those of this work, the conclusion is that the mobility is the same in diffused and uniformly doped silicon.

## 6. RESULTS FOR BORON-DOPED SILICON

Table 5 gives the data for boron-doped silicon derived from measurements on test patterns. The items listed and the symbols used are the same as those for table 1 except for the hole density,  $p$ , which was obtained from the dopant density using the ionization percentages calculated by Li [37]. Table 6 gives data on boron-doped silicon slices obtained by the nuclear track technique (NTT) [38]. Table 7 lists the results obtained from Hall effect measurements at both 23°C and 300 K. For calculating the hole density, the scattering factor was taken equal to 0.8 as discussed in section 4. This value was also used to obtain hole density from the Hall measurements of Chapman *et al.* [39] and Crowder [40].

Figure 7 is a graph of the product of resistivity and dopant density as a function of resistivity at 300 K. The NTT results are seen to be in good

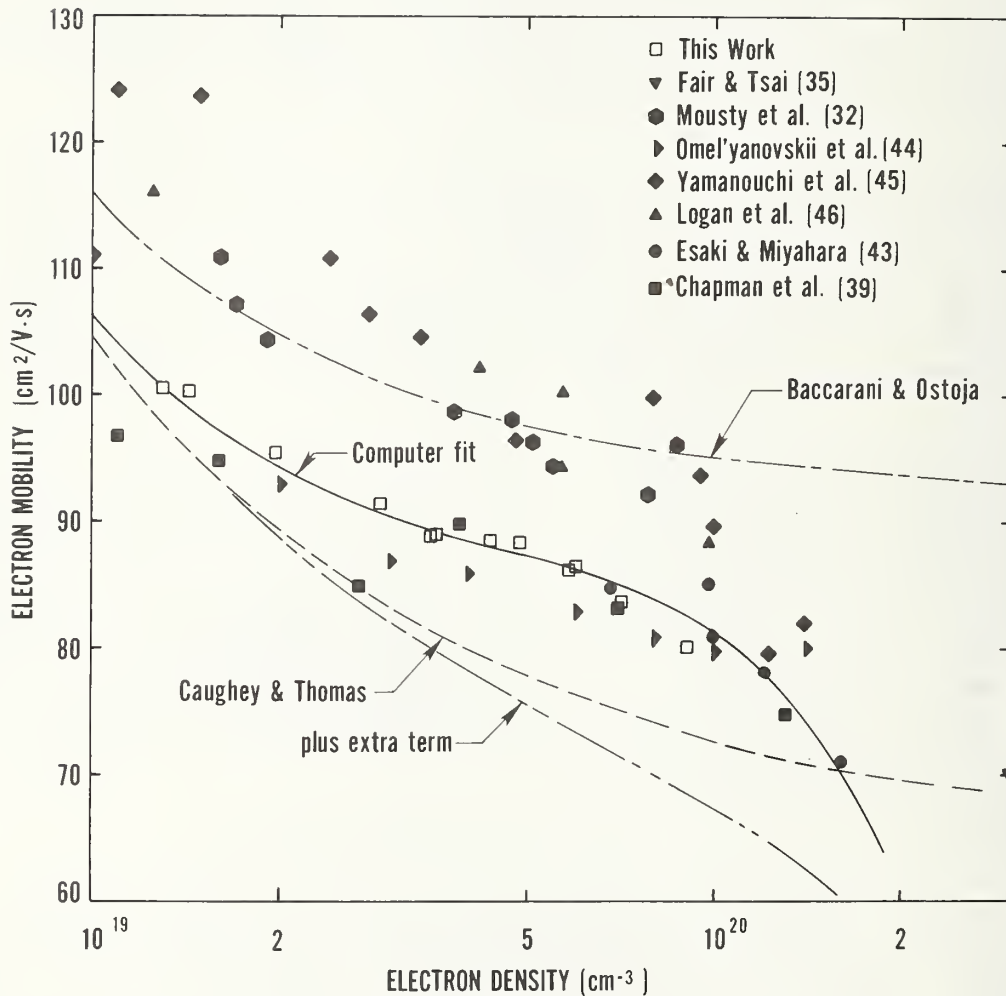


Figure 6. Electron mobility determined from Hall effect measurements for electron densities greater than  $10^{19}$   $\text{cm}^{-3}$ . The computer fit to the data of this work lies between the mobility expressions of Caughey and Thomas [1] and Baccarani and Ostoja [3]. The extra term in the modified Caughey and Thomas expression is given by Plunkett *et al.* [34].

Table 5. Data for Boron-Doped Silicon Obtained from Test Patterns.

| Wafer Identification                             | Site                     | N<br>cm <sup>-3</sup>    | $\rho_{23^\circ\text{C}}$<br>$\Omega\cdot\text{cm}$ | $\rho_{300\text{ K}}$<br>$\Omega\cdot\text{cm}$ | P<br>cm <sup>-3</sup>    | $\mu_{23^\circ\text{C}}$<br>cm <sup>2</sup> /V·s | $\mu_{300\text{ K}}$<br>cm <sup>2</sup> /V·s |
|--|--------------------------|--------------------------|---|---|--------------------------|--|--|
| B94B-3<br>$\rho_i = 94.0$<br>NBS-4<br>D = 432.8  | -1,1                     | 1.284 x 10 <sup>14</sup> | 94.68   | 97.85   | 1.284 x 10 <sup>14</sup> | 513.4  | 496.8  |
|  | 0,1                      | 1.362 x 10 <sup>14</sup> | 97.50   | 100.77  | 1.362 x 10 <sup>14</sup> | 470.0  | 454.8  |
|  | 1,1                      | 1.266 x 10 <sup>14</sup> | 96.48   | 99.71   | 1.266 x 10 <sup>14</sup> | 511.0  | 494.4  |
|  | -1,0                     | 1.362 x 10 <sup>14</sup> | 98.00   | 101.28  | 1.362 x 10 <sup>14</sup> | 467.6  | 452.5  |
|  | 0,0                      | 1.373 x 10 <sup>14</sup> | 99.62   | 102.96  | 1.373 x 10 <sup>14</sup> | 456.3  | 441.5  |
|  | 1,0                      | 1.313 x 10 <sup>14</sup> | 94.80   | 97.98   | 1.313 x 10 <sup>14</sup> | 501.4  | 485.2  |
|  | 1,-1                     | 1.328 x 10 <sup>14</sup> | 97.66   | 100.93  | 1.328 x 10 <sup>14</sup> | 481.2  | 465.7  |
| 0,-1   | 1.310 x 10 <sup>14</sup> | 96.35                    | 99.28   | 1.310 x 10 <sup>14</sup>                        | 494.5                    | 479.9  |  |
| Avg.   |                          | 1.325 x 10 <sup>14</sup> | 96.89   | 100.10  | 1.325 x 10 <sup>14</sup> | 486.9 ± 21.3                                     | 471.4 ± 20.7                                 |
| B49B-3<br>$\rho_i = 48.8$<br>NBS-4<br>D = 432.8  | -1,1                     | 2.547 x 10 <sup>14</sup> | 50.99   | 52.68   | 2.547 x 10 <sup>14</sup> | 480.6  | 465.2  |
|  | 0,1                      | 2.537 x 10 <sup>14</sup> | 49.42   | 51.06   | 2.537 x 10 <sup>14</sup> | 497.8  | 481.8  |
|  | 1,1                      | 2.640 x 10 <sup>14</sup> | 49.26   | 50.89   | 2.640 x 10 <sup>14</sup> | 479.9  | 464.6  |
|  | -1,0                     | 2.625 x 10 <sup>14</sup> | 49.30   | 50.93   | 2.625 x 10 <sup>14</sup> | 482.3  | 466.9  |
|  | 0,0                      | 2.648 x 10 <sup>14</sup> | 49.50   | 51.14   | 2.648 x 10 <sup>14</sup> | 476.2  | 460.9  |
|  | 1,0                      | 2.608 x 10 <sup>14</sup> | 49.66   | 51.30   | 2.608 x 10 <sup>14</sup> | 481.9  | 466.5  |
|  | Avg.                     |                          | 2.601 x 10 <sup>14</sup>                            | 49.69   | 51.33                    | 2.601 x 10 <sup>14</sup>                         | 483.1 ± 7.5                                  |
| C21B-2<br>$\rho_i = 22.0$<br>NBS-4<br>D = 433.3  | -1,1                     | 6.258 x 10 <sup>14</sup> | 20.79   | 21.48   | 6.258 x 10 <sup>14</sup> | 479.7  | 464.3  |
|  | 0,1                      | 6.267 x 10 <sup>14</sup> | 20.81   | 21.50   | 6.267 x 10 <sup>14</sup> | 478.6  | 463.2  |
|  | 1,1                      | 6.454 x 10 <sup>14</sup> | 20.57   | 21.25   | 6.454 x 10 <sup>14</sup> | 470.1  | 455.1  |
|  | -1,0                     | 6.248 x 10 <sup>14</sup> | 20.80   | 21.49   | 6.248 x 10 <sup>14</sup> | 488.1  | 464.8  |
|  | 0,0                      | 6.203 x 10 <sup>14</sup> | 20.82   | 21.51   | 6.203 x 10 <sup>14</sup> | 483.3  | 467.8  |
|  | 1,0                      | 6.219 x 10 <sup>14</sup> | 20.54   | 21.22   | 6.219 x 10 <sup>14</sup> | 488.6  | 473.0  |
|  | Avg.                     |                          | 6.275 x 10 <sup>14</sup>                            | 20.72   | 21.41                    | 6.275 x 10 <sup>14</sup>                         | 481.4 ± 6.9                                  |
| B9.0B-3<br>$\rho_i = 9.0$<br>NBS-4<br>D = 433.3  | 0,0                      | 1.489 x 10 <sup>15</sup> | 8.971   | 9.254   | 1.489 x 10 <sup>15</sup> | 467.2  | 453.0  |
|  | 1,0                      | 1.453 x 10 <sup>15</sup> | 8.911   | 9.192   | 1.453 x 10 <sup>15</sup> | 482.0  | 467.3  |
|  | 1,1                      | 1.488 x 10 <sup>15</sup> | 8.997   | 9.281   | 1.488 x 10 <sup>15</sup> | 466.2  | 451.9  |
|  | -1,0                     | 1.478 x 10 <sup>15</sup> | 8.948   | 9.230   | 1.478 x 10 <sup>15</sup> | 471.9  | 457.5  |
|  | -2,0                     | 1.479 x 10 <sup>15</sup> | 8.848   | 9.127   | 1.479 x 10 <sup>15</sup> | 476.9  | 462.4  |
|  | -1,2                     | 1.489 x 10 <sup>15</sup> | 8.900   | 9.181   | 1.489 x 10 <sup>15</sup> | 471.0  | 456.6  |
|  | 0,2                      | 1.487 x 10 <sup>15</sup> | 8.994   | 9.278   | 1.487 x 10 <sup>15</sup> | 466.7  | 452.4  |
|  | 1,2                      | 1.455 x 10 <sup>15</sup> | 8.966   | 9.249   | 1.455 x 10 <sup>15</sup> | 478.4  | 463.8  |
|  | Avg.                     |                          | 1.477 x 10 <sup>15</sup>                            | 8.942   | 9.224                    | 1.477 x 10 <sup>15</sup>                         | 472.5 ± 6.0                                  |
| B5.7B-4<br>$\rho_i = 5.7$<br>NBS-4<br>D = 433.8  | -1,1                     | 2.307 x 10 <sup>15</sup> | 5.753   | 5.932   | 2.300 x 10 <sup>15</sup> | 471.7  | 457.5  |
|  | 0,1                      | 2.294 x 10 <sup>15</sup> | 5.795   | 5.976   | 2.287 x 10 <sup>15</sup> | 470.9  | 456.7  |
|  | 1,1                      | 2.333 x 10 <sup>15</sup> | 5.767   | 5.947   | 2.326 x 10 <sup>15</sup> | 465.3  | 451.2  |
|  | -1,0                     | 2.312 x 10 <sup>15</sup> | 5.742   | 5.921   | 2.305 x 10 <sup>15</sup> | 471.6  | 457.3  |
|  | 0,0                      | 2.353 x 10 <sup>15</sup> | 5.648   | 5.824   | 2.346 x 10 <sup>15</sup> | 471.0  | 456.8  |
|  | 1,0                      | 2.342 x 10 <sup>15</sup> | 5.731   | 5.910   | 2.335 x 10 <sup>15</sup> | 466.4  | 452.3  |
|  | Avg.                     |                          | 2.324 x 10 <sup>15</sup>                            | 5.739   | 5.918                    | 2.317 x 10 <sup>15</sup>                         | 469.5 ± 2.9                                  |
| B3.0B-3<br>$\rho_i = 3.0$<br>NBS-4<br>D = 433.3  | -1,1                     | 4.756 x 10 <sup>15</sup> | 2.946   | 3.037   | 4.733 x 10 <sup>15</sup> | 447.6  | 434.2  |
|  | 0,1                      | 4.731 x 10 <sup>15</sup> | 2.949   | 3.040   | 4.708 x 10 <sup>15</sup> | 449.5  | 436.1  |
|  | -1,0                     | 4.643 x 10 <sup>15</sup> | 2.974   | 3.066   | 4.620 x 10 <sup>15</sup> | 454.3  | 440.6  |
|  | 0,0                      | 4.689 x 10 <sup>15</sup> | 2.967   | 3.059   | 4.666 x 10 <sup>15</sup> | 450.8  | 437.3  |
|  | 1,0                      | 4.673 x 10 <sup>15</sup> | 2.975   | 3.067   | 4.650 x 10 <sup>15</sup> | 451.2  | 437.6  |
|  | -1,-1                    | 4.663 x 10 <sup>15</sup> | 3.001   | 3.094   | 4.640 x 10 <sup>15</sup> | 448.2  | 434.8  |
|  | Avg.                     |                          | 4.693 x 10 <sup>15</sup>                            | 2.969   | 3.061                    | 4.670 x 10 <sup>15</sup>                         | 450.3 ± 2.4                                  |
| B1.8B-2<br>$\rho_i = 1.79$<br>NBS-4<br>D = 432.8 | -1,1                     | 8.135 x 10 <sup>15</sup> | 1.748   | 1.799   | 8.070 x 10 <sup>15</sup> | 442.5  | 429.9  |
|  | 0,1                      | 8.035 x 10 <sup>15</sup> | 1.772   | 1.823   | 7.971 x 10 <sup>15</sup> | 441.9  | 429.5  |
|  | 1,1                      | 7.913 x 10 <sup>15</sup> | 1.775   | 1.827   | 7.850 x 10 <sup>15</sup> | 447.9  | 435.2  |
|  | -1,0                     | 8.052 x 10 <sup>15</sup> | 1.764   | 1.814   | 7.988 x 10 <sup>15</sup> | 442.9  | 430.7  |
|  | 0,0                      | 7.906 x 10 <sup>15</sup> | 1.778   | 1.829   | 7.843 x 10 <sup>15</sup> | 447.6  | 435.1  |
|  | 1,0                      | 7.971 x 10 <sup>15</sup> | 1.775   | 1.826   | 7.907 x 10 <sup>15</sup> | 444.7  | 432.3  |
|  | Avg.                     |                          | 8.002 x 10 <sup>15</sup>                            | 1.769   | 1.820                    | 7.938 x 10 <sup>15</sup>                         | 444.6 ± 2.6                                  |

Table 5 - Continued

| Wafer Identification                               | Site                     | N<br>cm <sup>-3</sup>    | $\rho_{23^\circ\text{C}}$<br>$\Omega \cdot \text{cm}$ | $\rho_{300\text{ K}}$<br>$\Omega \cdot \text{cm}$ | p<br>cm <sup>-3</sup>    | $\mu_{23^\circ\text{C}}$<br>cm <sup>2</sup> /V·s | $\mu_{300\text{ K}}$<br>cm <sup>2</sup> /V·s |
|--|--------------------------|--------------------------|---|---|--------------------------|--|--|
| B1.1B-3<br>$\rho_i = 1.14$<br>NBS-3<br>D = 433.1   | -1,1                     | 1.312 x 10 <sup>16</sup> | 1.141   | 1.173   | 1.297 x 10 <sup>16</sup> | 421.8  | 410.2  |
|  | 1,1                      | 1.262 x 10 <sup>16</sup> | 1.134   | 1.166   | 1.247 x 10 <sup>16</sup> | 441.4  | 429.3  |
|  | -2,0                     | 1.281 x 10 <sup>16</sup> | 1.132   | 1.164   | 1.266 x 10 <sup>16</sup> | 435.5  | 423.5  |
|  | 1,0                      | 1.279 x 10 <sup>16</sup> | 1.138   | 1.170   | 1.264 x 10 <sup>16</sup> | 433.9  | 422.0  |
|  | 2,0                      | 1.281 x 10 <sup>16</sup> | 1.146   | 1.178   | 1.266 x 10 <sup>16</sup> | 430.2  | 418.5  |
|  | 0,-1                     | 1.270 x 10 <sup>16</sup> | 1.132   | 1.164   | 1.255 x 10 <sup>16</sup> | 439.3  | 427.3  |
| Avg.   | 1.281 x 10 <sup>16</sup> | 1.137                    | 1.169   | 1.266 x 10 <sup>16</sup>                          | 433.7 ± 7.0              | 421.8 ± 6.9                                      |  |
| B0.81B-1<br>$\rho_i = 0.81$<br>NBS-4<br>D = 433.3  | -1,2                     | 1.908 x 10 <sup>16</sup> | 0.813   | 0.835   | 1.874 x 10 <sup>16</sup> | 409.7  | 398.9  |
|  | 0,2                      | 1.908 x 10 <sup>16</sup> | 0.805   | 0.827   | 1.874 x 10 <sup>16</sup> | 413.7  | 402.7  |
|  | 1,2                      | 1.886 x 10 <sup>16</sup> | 0.802   | 0.824   | 1.852 x 10 <sup>16</sup> | 420.2  | 409.0  |
|  | -1,1                     | 1.901 x 10 <sup>16</sup> | 0.800   | 0.822   | 1.867 x 10 <sup>16</sup> | 417.9  | 406.7  |
|  | 1,1                      | 1.855 x 10 <sup>16</sup> | 0.810   | 0.832   | 1.822 x 10 <sup>16</sup> | 422.9  | 411.7  |
|  | 0,0                      | 1.896 x 10 <sup>16</sup> | 0.802   | 0.824   | 1.862 x 10 <sup>16</sup> | 418.0  | 407.0  |
| 1,0  | 1.909 x 10 <sup>16</sup> | 0.814                    | 0.836   | 1.875 x 10 <sup>16</sup>                          | 408.9                    | 398.2  |  |
| -1,-1  | 1.871 x 10 <sup>16</sup> | 0.810                    | 0.832   | 1.837 x 10 <sup>16</sup>                          | 419.5                    | 408.4  |  |
| Avg.   | 1.892 x 10 <sup>16</sup> | 0.807                    | 0.829   | 1.858 x 10 <sup>16</sup>                          | 416.4 ± 5.1              | 405.3 ± 4.9                                      |  |
| D0.58B-2<br>$\rho_i = 0.58$<br>NBS-3<br>D = 433.6  | -2,0                     | 2.890 x 10 <sup>16</sup> | 0.5718  | 0.5867  | 2.818 x 10 <sup>16</sup> | 387.3  | 377.5  |
|  | 0,0                      | 2.877 x 10 <sup>16</sup> | 0.5723  | 0.5872  | 2.805 x 10 <sup>16</sup> | 388.8  | 378.9  |
|  | 1,0                      | 2.897 x 10 <sup>16</sup> | 0.5713  | 0.5862  | 2.825 x 10 <sup>16</sup> | 386.7  | 376.9  |
|  | -2,-1                    | 2.870 x 10 <sup>16</sup> | 0.5777  | 0.5927  | 2.799 x 10 <sup>16</sup> | 386.0  | 376.2  |
|  | -1,-1                    | 2.906 x 10 <sup>16</sup> | 0.5718  | 0.5867  | 2.834 x 10 <sup>16</sup> | 385.2  | 375.4  |
|  | 1,-1                     | 2.922 x 10 <sup>16</sup> | 0.5677  | 0.5825  | 2.849 x 10 <sup>16</sup> | 385.9  | 376.1  |
| Avg.   | 2.894 x 10 <sup>16</sup> | 0.5721                   | 0.5870  | 2.822 x 10 <sup>16</sup>                          | 386.7 ± 1.3              | 376.8 ± 1.2                                      |  |
| E0.43B-3<br>$\rho_i = 0.43$<br>NBS-4<br>D = 433.8  | -1,1                     | 4.196 x 10 <sup>16</sup> | 0.4068  | 0.4165  | 4.053 x 10 <sup>16</sup> | 378.6  | 369.7  |
|  | 0,1                      | 4.311 x 10 <sup>16</sup> | 0.4104  | 0.4202  | 4.164 x 10 <sup>16</sup> | 365.2  | 356.7  |
|  | 1,1                      | 4.215 x 10 <sup>16</sup> | 0.4072  | 0.4169  | 4.071 x 10 <sup>16</sup> | 376.5  | 367.7  |
|  | -1,0                     | 4.196 x 10 <sup>16</sup> | 0.4078  | 0.4175  | 4.053 x 10 <sup>16</sup> | 377.6  | 368.9  |
|  | 0,0                      | 4.139 x 10 <sup>16</sup> | 0.4179  | 0.4279  | 3.998 x 10 <sup>16</sup> | 373.6  | 364.8  |
|  | 1,0                      | 4.109 x 10 <sup>16</sup> | 0.4071  | 0.4168  | 3.969 x 10 <sup>16</sup> | 386.3  | 377.3  |
| Avg.   | 4.194 x 10 <sup>16</sup> | 0.4095                   | 0.4193  | 4.051 x 10 <sup>16</sup>                          | 376.3 ± 6.9              | 367.5 ± 6.7                                      |  |
| B0.32B-2<br>$\rho_i = 0.32$<br>NBS-4<br>D = 433.8  | -1,1                     | 5.927 x 10 <sup>16</sup> | 0.3085  | 0.3154  | 5.661 x 10 <sup>16</sup> | 357.4  | 349.6  |
|  | 0,1                      | 5.861 x 10 <sup>16</sup> | 0.3136  | 0.3206  | 5.598 x 10 <sup>16</sup> | 355.5  | 347.8  |
|  | 1,1                      | 5.878 x 10 <sup>16</sup> | 0.3144  | 0.3214  | 5.614 x 10 <sup>16</sup> | 353.6  | 345.9  |
|  | -1,0                     | 5.987 x 10 <sup>16</sup> | 0.3105  | 0.3174  | 5.718 x 10 <sup>16</sup> | 351.5  | 343.9  |
|  | 0,0                      | 5.944 x 10 <sup>16</sup> | 0.3096  | 0.3165  | 5.677 x 10 <sup>16</sup> | 355.1  | 347.4  |
|  | 1,0                      | 5.911 x 10 <sup>16</sup> | 0.3096  | 0.3165  | 5.645 x 10 <sup>16</sup> | 357.1  | 349.3  |
| Avg.   | 5.918 x 10 <sup>16</sup> | 0.3110                   | 0.3180  | 5.646 x 10 <sup>16</sup>                          | 355.0 ± 2.2              | 347.3 ± 2.1                                      |  |
| B0.23B-2<br>$\rho_i = 0.22$<br>NBS-4<br>D = 433.8  | -1,1                     | 9.020 x 10 <sup>16</sup> | 0.2216  | 0.2261  | 8.461 x 10 <sup>16</sup> | 332.9  | 326.3  |
|  | 0,1                      | 8.890 x 10 <sup>16</sup> | 0.2236  | 0.2282  | 8.339 x 10 <sup>16</sup> | 334.7  | 328.0  |
|  | 1,1                      | 8.791 x 10 <sup>16</sup> | 0.2213  | 0.2258  | 8.246 x 10 <sup>16</sup> | 342.0  | 335.2  |
|  | -1,0                     | 8.775 x 10 <sup>16</sup> | 0.2234  | 0.2280  | 8.231 x 10 <sup>16</sup> | 339.4  | 332.6  |
|  | 0,0                      | 8.783 x 10 <sup>16</sup> | 0.2241  | 0.2287  | 8.239 x 10 <sup>16</sup> | 338.0  | 331.2  |
|  | 1,0                      | 9.166 x 10 <sup>16</sup> | 0.2161  | 0.2205  | 8.598 x 10 <sup>16</sup> | 335.9  | 329.2  |
| Avg.   | 8.904 x 10 <sup>16</sup> | 0.2217                   | 0.2262  | 8.352 x 10 <sup>16</sup>                          | 337.2 ± 3.3              | 330.4 ± 3.2                                      |  |
| B0.17B-1<br>$\rho_i = 0.165$<br>NBS-4<br>D = 433.8 | -1,1                     | 1.369 x 10 <sup>17</sup> | 0.1585  | 0.1614  | 1.254 x 10 <sup>17</sup> | 314.0  | 308.4  |
|  | 0,1                      | 1.366 x 10 <sup>17</sup> | 0.1604  | 0.1634  | 1.252 x 10 <sup>17</sup> | 310.8  | 305.1  |
|  | 1,1                      | 1.338 x 10 <sup>17</sup> | 0.1603  | 0.1633  | 1.226 x 10 <sup>17</sup> | 317.6  | 311.8  |
|  | -1,0                     | 1.377 x 10 <sup>17</sup> | 0.1588  | 0.1617  | 1.262 x 10 <sup>17</sup> | 311.4  | 305.9  |
|  | 0,0                      | 1.395 x 10 <sup>17</sup> | 0.1586  | 0.1615  | 1.278 x 10 <sup>17</sup> | 307.9  | 302.4  |
|  | 1,0                      | 1.397 x 10 <sup>17</sup> | 0.1595  | 0.1624  | 1.280 x 10 <sup>17</sup> | 305.7  | 300.3  |
| Avg.   | 1.374 x 10 <sup>17</sup> | 0.1594                   | 0.1623  | 1.259 x 10 <sup>17</sup>                          | 311.2 ± 4.2              | 305.6 ± 4.1                                      |  |

Table 5 - Continued

| Wafer Identification                                | Site  | N<br>cm <sup>-3</sup>    | $\rho_{23^\circ\text{C}}$<br>$\Omega\cdot\text{cm}$ | $\rho_{300\text{ K}}$<br>$\Omega\cdot\text{cm}$ | p<br>cm <sup>-3</sup>    | $\mu_{23^\circ\text{C}}$<br>cm <sup>2</sup> /V·s | $\mu_{300\text{ K}}$<br>cm <sup>2</sup> /V·s |
|---|-------|--------------------------|---|---|--------------------------|--|--|
| B0.097B-2<br>$\rho_i = 0.096$<br>NBS-4<br>D = 433.8 | -1,1  | 2.717 x 10 <sup>17</sup> | 0.0968  | 0.0982  | 2.355 x 10 <sup>17</sup> | 273.8  | 269.9  |
|   | 0,1   | 1.895 x 10 <sup>17</sup> | 0.0952  | 0.0966  | 2.509 x 10 <sup>17</sup> | 261.3  | 257.5  |
|   | 1,1   | 2.935 x 10 <sup>17</sup> | 0.0942  | 0.0955  | 2.544 x 10 <sup>17</sup> | 260.4  | 256.9  |
|   | -1,0  | 2.848 x 10 <sup>17</sup> | 0.0954  | 0.0968  | 2.469 x 10 <sup>17</sup> | 265.0  | 261.1  |
|   | 0,0   | 2.910 x 10 <sup>17</sup> | 0.0945  | 0.0958  | 2.522 x 10 <sup>17</sup> | 261.9  | 258.3  |
|   | 1,0   | 2.862 x 10 <sup>17</sup> | 0.0942  | 0.0955  | 2.481 x 10 <sup>17</sup> | 267.1  | 263.4  |
|   | Avg.  | 2.861 x 10 <sup>17</sup> | 0.0951  | 0.0964  | 2.480 x 10 <sup>17</sup> | 264.9 ± 5.0                                      | 261.2 ± 4.9                                  |
| B0.090B-2<br>$\rho_i = 0.090$<br>NBS-3<br>D = 433.6 | -1,3  | 3.189 x 10 <sup>17</sup> | 0.0889  | 0.0901  | 2.742 x 10 <sup>17</sup> | 256.0  | 252.6  |
|   | 0,3   | 3.242 x 10 <sup>17</sup> | 0.0891  | 0.0903  | 2.788 x 10 <sup>17</sup> | 251.3  | 247.9  |
|   | -2,2  | 3.132 x 10 <sup>17</sup> | 0.0893  | 0.0905  | 2.693 x 10 <sup>17</sup> | 259.5  | 256.1  |
|   | 0,2   | 3.210 x 10 <sup>17</sup> | 0.0893  | 0.0905  | 2.760 x 10 <sup>17</sup> | 253.2  | 249.9  |
|   | 1,2   | 3.147 x 10 <sup>17</sup> | 0.0891  | 0.0903  | 2.706 x 10 <sup>17</sup> | 258.9  | 255.4  |
|   | 0,1   | 3.200 x 10 <sup>17</sup> | 0.0890  | 0.0902  | 2.752 x 10 <sup>17</sup> | 254.8  | 251.4  |
|   | 1,1   | 3.219 x 10 <sup>17</sup> | 0.0890  | 0.0902  | 2.768 x 10 <sup>17</sup> | 253.4  | 250.0  |
|   | Avg.  | 3.191 x 10 <sup>17</sup> | 0.0891  | 0.0903  | 2.744 x 10 <sup>17</sup> | 255.3 ± 3.0                                      | 251.9 ± 3.0                                  |
| B0.054B-3<br>$\rho_i = 0.055$<br>NBS-4<br>D = 433.8 | -1,1  | 7.260 x 10 <sup>17</sup> | 0.0548  | 0.0553  | 5.757 x 10 <sup>17</sup> | 197.8  | 196.0  |
|   | 0,1   | 7.183 x 10 <sup>17</sup> | 0.0548  | 0.0553  | 5.696 x 10 <sup>17</sup> | 200.0  | 198.1  |
|   | 1,1   | 7.016 x 10 <sup>17</sup> | 0.0553  | 0.0558  | 5.563 x 10 <sup>17</sup> | 202.9  | 201.1  |
|   | 1,0   | 7.159 x 10 <sup>17</sup> | 0.0549  | 0.0554  | 5.677 x 10 <sup>17</sup> | 200.3  | 198.5  |
|   | -1,-1 | 7.128 x 10 <sup>17</sup> | 0.0546  | 0.0551  | 5.652 x 10 <sup>17</sup> | 202.2  | 200.4  |
|   | 0,-1  | 7.109 x 10 <sup>17</sup> | 0.0546  | 0.0551  | 5.637 x 10 <sup>17</sup> | 202.8  | 200.9  |
|   | 1,-1  | 7.318 x 10 <sup>17</sup> | 0.0546  | 0.0551  | 5.803 x 10 <sup>17</sup> | 197.0  | 195.2  |
|   | Avg.  | 7.168 x 10 <sup>17</sup> | 0.0548  | 0.0553  | 5.684 x 10 <sup>17</sup> | 200.4 ± 2.4                                      | 198.6 ± 2.4                                  |

Table 6. Data for Silicon Slices with the Boron Density Determined by the Nuclear Track Technique.

| Slice Identification | Run   | N<br>cm <sup>-3</sup>   | $\rho_{23^\circ\text{C}}$<br>$\Omega \cdot \text{cm}$ | $\rho_{300\text{ K}}$<br>$\Omega \cdot \text{cm}$ | p<br>cm <sup>-3</sup>   | $\mu_{23^\circ\text{C}}$<br>cm <sup>2</sup> /V·s | $\mu_{300\text{ K}}$<br>cm <sup>2</sup> /V·s |
|----------------------|-------|-------------------------|---|---|-------------------------|--|--|
| A7                   | 1     | 1.02 x 10 <sup>15</sup> | 10.9  | 11.2  | 1.02 x 10 <sup>15</sup> | 561  | 546  |
|                      | 2     | 1.33 x 10 <sup>15</sup> | 10.9  | 11.2  | 1.33 x 10 <sup>15</sup> | 431  | 419  |
|                      | Avg.  | 1.18 x 10 <sup>15</sup> | 10.9  | 11.2  | 1.18 x 10 <sup>15</sup> | 496  | 482  |
| 521-5                | 1     | 1.84 x 10 <sup>15</sup> | 10.8  | 11.1  | 1.84 x 10 <sup>15</sup> | 314  | 306  |
|                      | 2     | 1.76 x 10 <sup>15</sup> | 10.8  | 11.1  | 1.76 x 10 <sup>15</sup> | 328  | 320  |
|                      | 3     | 1.71 x 10 <sup>15</sup> | 10.8  | 11.1  | 1.71 x 10 <sup>15</sup> | 338  | 329  |
|                      | Avg.  | 1.77 x 10 <sup>15</sup> | 10.8  | 11.1  | 1.77 x 10 <sup>15</sup> | 327  | 318  |
| 521-22               | 1     | 5.01 x 10 <sup>15</sup> | 3.08  | 3.17  | 4.99 x 10 <sup>15</sup> | 406  | 395  |
|                      | 2     | 4.90 x 10 <sup>15</sup> | 3.01  | 3.10  | 4.88 x 10 <sup>15</sup> | 425  | 413  |
|                      | Avg.  | 4.95 x 10 <sup>15</sup> | 3.04  | 3.13  | 4.93 x 10 <sup>15</sup> | 415  | 404  |
| 521-21               | 1     | 6.89 x 10 <sup>15</sup> | 1.85  | 1.90  | 6.84 x 10 <sup>15</sup> | 493  | 480  |
| A6                   | 1     | 7.17 x 10 <sup>15</sup> | 1.84  | 1.89  | 7.11 x 10 <sup>15</sup> | 477  | 465  |
| 521-53               | 1     | 2.26 x 10 <sup>15</sup> | 0.71  | 0.73  | 2.21 x 10 <sup>15</sup> | 398  | 387  |
|                      | 2     | 2.26 x 10 <sup>15</sup> | 0.71  | 0.73  | 2.21 x 10 <sup>15</sup> | 398  | 387  |
|                      | 3     | 2.27 x 10 <sup>15</sup> | 0.71  | 0.73  | 2.22 x 10 <sup>15</sup> | 396  | 385  |
|                      | Avg.  | 2.26 x 10 <sup>15</sup> | 0.71  | 0.73  | 2.21 x 10 <sup>15</sup> | 397  | 386  |
| 521-4                | 1     | 6.00 x 10 <sup>15</sup> | 0.28  | 0.29  | 5.72 x 10 <sup>15</sup> | 390  | 376  |
|                      | 2     | 6.10 x 10 <sup>15</sup> | 0.277   | 0.283   | 5.82 x 10 <sup>15</sup> | 387  | 379  |
|                      | Avg.  | 6.05 x 10 <sup>15</sup> | 0.28  | 0.29  | 5.77 x 10 <sup>15</sup> | 388  | 377  |
| 521-76               | 1     | 1.29 x 10 <sup>17</sup> | 0.221   | 0.225   | 1.19 x 10 <sup>17</sup> | 237  | 233  |
|                      | 2     | 1.12 x 10 <sup>17</sup> | 0.221   | 0.225   | 1.03 x 10 <sup>17</sup> | 274  | 269  |
|                      | Avg.  | 1.21 x 10 <sup>17</sup> | 0.221   | 0.225   | 1.11 x 10 <sup>17</sup> | 225  | 251  |
| 521-57               | 1     | 4.55 x 10 <sup>17</sup> | 0.0959  | 0.0972  | 3.78 x 10 <sup>17</sup> | 172.2  | 169.9  |
|                      | 2     | 4.48 x 10 <sup>17</sup> | 0.0959  | 0.0972  | 3.72 x 10 <sup>17</sup> | 175.0  | 172.6  |
|                      | Avg.  | 4.52 x 10 <sup>17</sup> | 0.0959  | 0.0972  | 3.75 x 10 <sup>17</sup> | 173.6  | 171.2  |
| 521-62               | 1     | 7.29 x 10 <sup>17</sup> | 0.054   | 0.0545  | 5.78 x 10 <sup>17</sup> | 200.0  | 198.2  |
|                      | 2     | 6.67 x 10 <sup>17</sup> | 0.0558  | 0.0563  | 5.29 x 10 <sup>17</sup> | 211.5  | 209.6  |
|                      | 3     | 7.41 x 10 <sup>17</sup> | 0.0558  | 0.0563  | 5.88 x 10 <sup>17</sup> | 190.3  | 188.6  |
|                      | Avg.† | 7.12 x 10 <sup>17</sup> | 0.0552  | 0.0557  | 5.65 x 10 <sup>17</sup> | 200.6  | 198.8  |
| 521-58               | 1     | 4.24 x 10 <sup>18</sup> | 0.0204  | 0.0204  | 4.24 x 10 <sup>18</sup> | 72.2   | 72.2   |
|                      | 2     | 3.89 x 10 <sup>18</sup> | 0.0204  | 0.0204  | 3.89 x 10 <sup>18</sup> | 78.7   | 78.7   |
|                      | Avg.  | 4.06 x 10 <sup>18</sup> | 0.0204  | 0.0204  | 4.06 x 10 <sup>18</sup> | 75.5   | 75.5   |
| A3                   | 1†    | 5.17 x 10 <sup>18</sup> | 0.0149  | 0.0149  | 5.17 x 10 <sup>18</sup> | 81.0   | 81.0   |
| 521-44               | 1     | 5.96 x 10 <sup>18</sup> | 0.0130  | 0.0130  | 5.96 x 10 <sup>18</sup> | 80.6   | 80.6   |
|                      | 2     | 5.80 x 10 <sup>18</sup> | 0.0130  | 0.0130  | 5.80 x 10 <sup>18</sup> | 82.8   | 82.8   |
|                      | Avg.  | 5.88 x 10 <sup>18</sup> | 0.0130  | 0.0130  | 5.88 x 10 <sup>18</sup> | 81.7   | 81.7   |

†Used for computer curve fit.

Table 6 - Continued

| Slice Identification | Run                     | N<br>-3<br>cm           | $\rho_{23^\circ\text{C}}$<br>$\Omega \cdot \text{cm}$ | $\rho_{300\text{ K}}$<br>$\Omega \cdot \text{cm}$ | P<br>-3<br>cm                 | $\mu_{23^\circ\text{C}}$<br>$\text{cm}^2/\text{V}\cdot\text{s}$ | $\mu_{300\text{ K}}$<br>$\text{cm}^2/\text{V}\cdot\text{s}$ |
|----------------------|-------------------------|-------------------------|---|---|-------------------------------|---|---|
| 521-23               | 1                       | 2.27 x 10 <sup>19</sup> | 0.0047  | 0.0047  | 2.27 x 10 <sup>19</sup>       | 58.5  | 58.5  |
|                      | 2                       | 2.14 x 10 <sup>19</sup> | 0.0047  | 0.0047  | 2.14 x 10 <sup>19</sup>       | 62.1  | 62.1  |
|                      | 3                       | 2.10 x 10 <sup>19</sup> | <u>0.0047</u>   | <u>0.0047</u>                                     | <u>2.10 x 10<sup>19</sup></u> | <u>63.2</u>   | <u>63.2</u>   |
|                      | Avg. †                  | 2.17 x 10 <sup>19</sup> | 0.0047  | 0.0047  | 2.17 x 10 <sup>19</sup>       | 61.3  | 61.3  |
| A2                   | 1                       | 2.89 x 10 <sup>19</sup> | 0.0040  | 0.0040  | 2.89 x 10 <sup>19</sup>       | 54.0  | 54.0  |
|                      | 2                       | 2.81 x 10 <sup>19</sup> | 0.0040  | 0.0040  | 2.81 x 10 <sup>19</sup>       | 55.5  | 55.5  |
|                      | 3                       | 2.58 x 10 <sup>19</sup> | 0.0040  | 0.0040  | 2.58 x 10 <sup>19</sup>       | 60.5  | 60.5  |
|                      | 4                       | 2.82 x 10 <sup>19</sup> | <u>0.0040</u>   | <u>0.0040</u>                                     | <u>2.82 x 10<sup>19</sup></u> | <u>55.3</u>   | <u>55.3</u>   |
| Avg. †               | 2.78 x 10 <sup>19</sup> | 0.0040                  | 0.0040  | 2.78 x 10 <sup>19</sup>                           | 56.3                          | 56.3  |   |
| 521-45               | 1                       | 2.80 x 10 <sup>19</sup> | 0.00294   | 0.00294   | 2.80 x 10 <sup>19</sup>       | 75.8  | 75.8  |
| 521-73               | 1                       | 4.42 x 10 <sup>19</sup> | 0.00176   | 0.00177   | 4.42 x 10 <sup>19</sup>       | 80.2  | 79.8  |
|                      | 2                       | 4.53 x 10 <sup>19</sup> | <u>0.00176</u>  | <u>0.00177</u>                                    | <u>4.53 x 10<sup>19</sup></u> | <u>78.3</u>   | <u>77.9</u>   |
|                      | Avg.                    | 4.47 x 10 <sup>19</sup> | 0.00176   | 0.00177   | 4.47 x 10 <sup>19</sup>       | 79.2  | 78.8  |
| 521-24               | 1                       | 1.00 x 10 <sup>20</sup> | 0.00105   | 0.00106   | 1.00 x 10 <sup>20</sup>       | 59.4  | 58.9  |
|                      | 2                       | 1.23 x 10 <sup>20</sup> | 0.00105   | 0.00106   | 1.23 x 10 <sup>20</sup>       | 48.3  | 47.9  |
|                      | 3                       | 1.23 x 10 <sup>20</sup> | <u>0.00105</u>  | <u>0.00106</u>                                    | <u>1.23 x 10<sup>20</sup></u> | <u>48.3</u>   | <u>47.9</u>   |
|                      | Avg. †                  | 1.15 x 10 <sup>20</sup> | 0.00105   | 0.00106   | 1.15 x 10 <sup>20</sup>       | 52.0  | 51.6  |

†Used for computer curve fit.

Table 7. Data for Boron-Doped Silicon Obtained from van der Pauw Specimens.

| Specimen No.               | T = 23°C                    |  |                              |  | T = 300 K                   |  |                              |  |
|----------------------------|-----------------------------|--|------------------------------|--|-----------------------------|--|------------------------------|--|
|                            | $R_H(\text{cm}^3/\text{C})$ | $p(\text{cm}^{-3})$                      | $\rho(\Omega\cdot\text{cm})$ | $\mu(\text{cm}^2/\text{V}\cdot\text{s})$ | $R_H(\text{cm}^3/\text{C})$ | $p(\text{cm}^{-3})$                      | $\rho(\Omega\cdot\text{cm})$ | $\mu(\text{cm}^2/\text{V}\cdot\text{s})$ |
| B0.010B-1                  | 0.5839                      | $8.550 \times 10^{18}$                   | 0.009625                     | 75.8                                     | 0.5823                      | $8.57 \times 10^{18}$                    | 0.009637                     | 75.6                                     |
| E0.0092B-1                 | 0.5175                      | $9.650 \times 10^{18}$                   | 0.008865                     | 73.0                                     | 0.5165                      | $9.67 \times 10^{18}$                    | 0.008873                     | 72.7                                     |
| A0.0082B-1                 | 0.4455                      | $1.121 \times 10^{19}$                   | 0.00798                      | 69.8                                     | 0.4465                      | $1.118 \times 10^{19}$                   | 0.00800                      | 69.8                                     |
| E0.0077B-2                 | 0.4044                      | $1.235 \times 10^{19}$                   | 0.00739                      | 68.4                                     | 0.4041                      | $1.236 \times 10^{19}$                   | 0.00741                      | 68.1                                     |
| A0.0072B-2                 | 0.3788                      | $1.318 \times 10^{19}$                   | 0.007064                     | 67.0                                     | 0.3784                      | $1.320 \times 10^{19}$                   | 0.007080                     | 66.8                                     |
| E0.0064B-1                 | 0.3163                      | $1.579 \times 10^{19}$                   | 0.006083                     | 65.0                                     | 0.3153                      | $1.584 \times 10^{19}$                   | 0.006100                     | 64.6                                     |
| A0.0061B-1                 | 0.3037                      | $1.644 \times 10^{19}$                   | 0.005932                     | 64.0                                     | 0.3020                      | $1.653 \times 10^{19}$                   | 0.005949                     | 63.5                                     |
| A0.0059B-1                 | 0.2883                      | $1.732 \times 10^{19}$                   | 0.005710                     | 63.1                                     | 0.2881                      | $1.733 \times 10^{19}$                   | 0.005727                     | 62.9                                     |
| A0.0059B-1C <sup>†</sup>   | <u>0.2927</u>               | <u><math>1.706 \times 10^{19}</math></u> | <u>0.005830</u>              | <u>62.8</u>                              | <u>0.2915</u>               | <u><math>1.713 \times 10^{19}</math></u> | <u>0.005845</u>              | <u>62.3</u>                              |
| Avg.                       | 0.2905                      | $1.719 \times 10^{19}$                   | 0.005770                     | 63.0                                     | 0.2898                      | $1.723 \times 10^{19}$                   | 0.005786                     | 62.6                                     |
| 0.005B-R7370               | 0.2572                      | $1.941 \times 10^{19}$                   | 0.00510                      | 63.1                                     | 0.2560                      | $1.950 \times 10^{19}$                   | 0.005145                     | 62.2                                     |
| 0.0043B-23-1               | 0.2030                      | $2.460 \times 10^{19}$                   | 0.00424                      | 59.8                                     | 0.2047                      | $2.439 \times 10^{19}$                   | 0.00426                      | 60.1                                     |
| 0.0030B-45-1               | 0.1305                      | $3.826 \times 10^{19}$                   | 0.002851                     | 57.2                                     | 0.1304                      | $3.829 \times 10^{19}$                   | 0.002866                     | 56.9                                     |
| B0.0019B-2                 | 0.0821                      | $6.080 \times 10^{19}$                   | 0.001849                     | 55.5                                     | 0.0826                      | $6.045 \times 10^{19}$                   | 0.001862                     | 55.5                                     |
| 0.0018B-73-1               | 0.0750                      | $6.660 \times 10^{19}$                   | 0.001701                     | 55.1                                     | 0.0743                      | $6.720 \times 10^{19}$                   | 0.001712                     | 54.3                                     |
| 0.0018B-73-1C <sup>†</sup> | <u>0.0751</u>               | <u><math>6.650 \times 10^{19}</math></u> | <u>0.001712</u>              | <u>54.8</u>                              | <u>0.0752</u>               | <u><math>6.640 \times 10^{19}</math></u> | <u>0.001723</u>              | <u>54.6</u>                              |
| Avg.                       | 0.0750                      | $6.655 \times 10^{19}$                   | 0.001707                     | 55.0                                     | 0.0747                      | $6.680 \times 10^{19}$                   | 0.001718                     | 54.4                                     |
| 0.0010B-24-1               | 0.0449                      | $1.112 \times 10^{20}$                   | 0.001047                     | 53.6                                     | 0.0446                      | $1.120 \times 10^{20}$                   | 0.001054                     | 52.9                                     |
| 0.0010B-74-1               | 0.0446                      | $1.120 \times 10^{20}$                   | 0.001036                     | 53.8                                     | 0.0449                      | $1.112 \times 10^{20}$                   | 0.001043                     | 53.8                                     |
| (repeat)                   | 0.0447                      | $1.117 \times 10^{20}$                   | 0.001033                     | 54.1                                     | 0.0448                      | $1.115 \times 10^{20}$                   | 0.001040                     | 53.8                                     |
| 0.0010B-74-1C <sup>†</sup> | <u>0.0446</u>               | <u><math>1.120 \times 10^{20}</math></u> | <u>0.001027</u>              | <u>54.3</u>                              | <u>0.0444</u>               | <u><math>1.125 \times 10^{20}</math></u> | <u>0.001034</u>              | <u>53.7</u>                              |
| Avg.                       | 0.0446                      | $1.119 \times 10^{20}$                   | 0.001032                     | 54.1                                     | 0.0447                      | $1.117 \times 10^{20}$                   | 0.001039                     | 53.8                                     |
| A0.00087B-1                | 0.0367                      | $1.361 \times 10^{20}$                   | 0.000851                     | 53.9                                     | 0.0360                      | $1.387 \times 10^{20}$                   | 0.000857                     | 52.5                                     |

<sup>†</sup>"C" denotes specimen in the shape of a Greek cross; all other specimens had shape shown in figure 3.



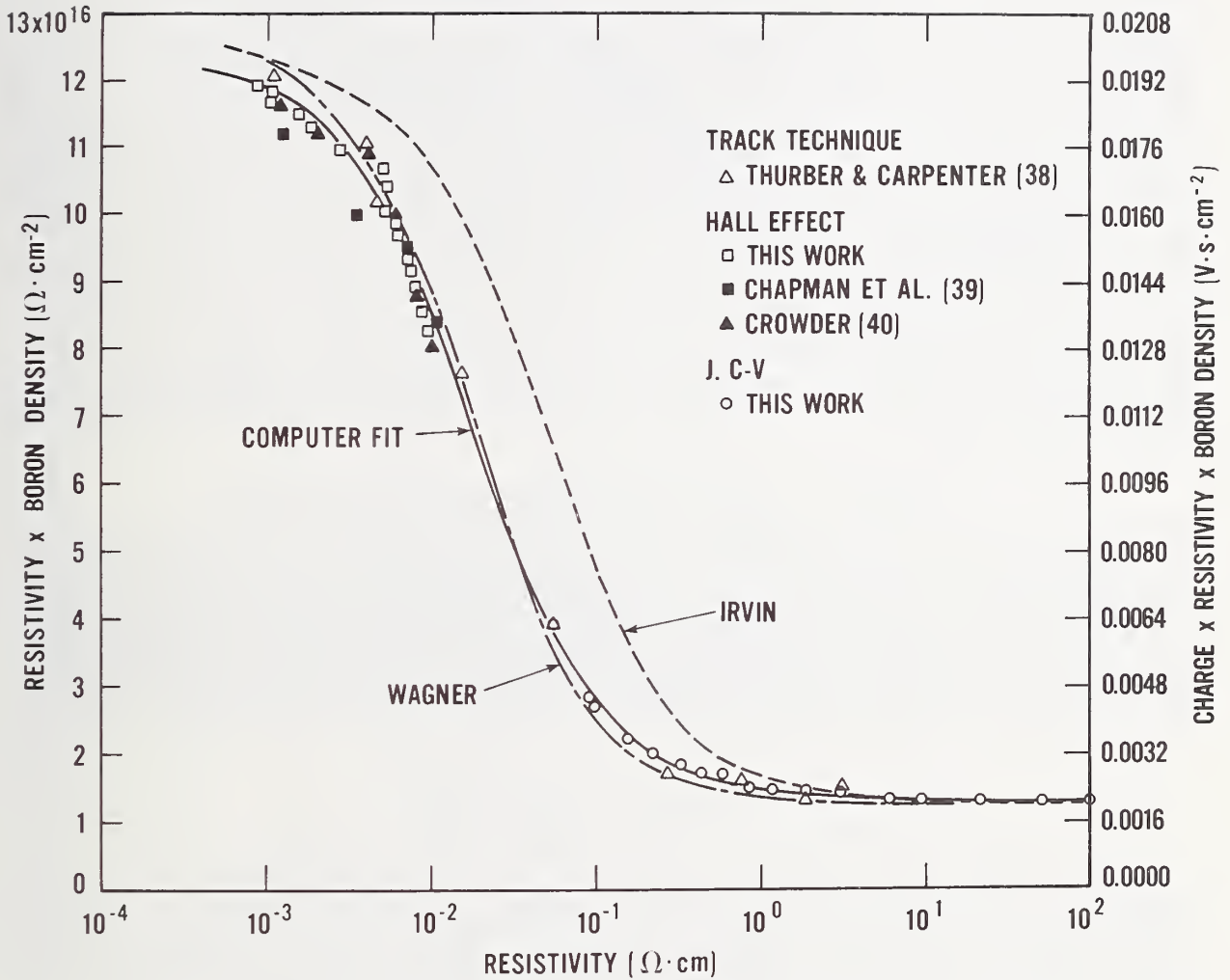


Figure 7. Resistivity-dopant density product as a function of resistivity at 300 K for boron-doped silicon. The junction capacitance voltage and Hall effect measurements are compared with the published work of Thurber and Carpenter [38], Chapman *et al.* [39], Crowder [40], Irvin [2], and Wagner [4]. The solid curve is an analytical fit to portions of these data as discussed in the text. Values of the product  $q\rho N$  are on the right ordinate.

agreement with both the Hall effect and the C-V data. The curves shown are the Irvin relationship for *p*-type silicon, the Wagner relationship for boron-implanted silicon, and an analytical curve fit to the data given in tables 5, 6, and 7. As is evident from the figure, the results obtained from measurements on boron-doped silicon depart considerably from the *p*-type Irvin curve.

Figure 8 is a plot of hole mobility as a function of hole density at 300 K. The fairly recent data of Tsao and Sah [41] are significantly lower than the data of this work. This may result from the fact that back-surface contact resistance can strongly affect resistivity values obtained from the spreading resistance structure used by Tsao and Sah. The Caughey and Thomas [1] curve is a fit to the Irvin relationship with the assumption that the hole density equals the dopant density. The same assumption was used to obtain the Wagner curve; however, it was not a point-by-point determination but simply a change in one parameter of the Caughey and Thomas expression as required to fit data on boron-implanted silicon. Just as the Irvin curve is a poor fit to the resistivity-dopant density data of this work, the Caughey and Thomas expression is a poor fit to the mobility data. The Wagner expression is considerably better, but there are still noticeable deviations with respect to the experimental data. The theoretical calculation of Li [37] in figure 8, valid for densities less than  $3 \times 10^{18} \text{ cm}^{-3}$ , is in excellent agreement with the C-V data of this work.

## 7. COMPUTER CURVE FITS FOR PHOSPHORUS-DOPED SILICON

The curve fits of the data were done using the DATAPLOT language [42] for the nonlinear least squares fitting. The simplest expression which gave a fit of the same precision as the uncertainty in the experimental data was the log of the resistivity-dopant density product equal to a third-degree polynomial divided by a third-degree polynomial. Therefore, the equation for fitting the resistivity-dopant density product was taken to have the form

$$\log_{10} (P/P_0) = \frac{A_0 + A_1 X + A_2 X^2 + A_3 X^3}{1 + B_1 X + B_2 X^2 + B_3 X^3}, \quad (1)$$

with  $P = q\rho N$  where  $q$  is the electronic charge,  $\rho$  is the resistivity, and  $N$  is the electrically active dopant density. The normalization factor,  $P_0$ , was taken equal to  $1 \text{ V}\cdot\text{s}/\text{cm}^2$ . Fits were made for both  $X = \log_{10} (\rho/\rho_0)$  and  $X = \log_{10} (N/N_0)$  with  $\rho_0 = 1 \Omega\cdot\text{cm}$  and  $N_0 = 10^{16} \text{ cm}^{-3}$ . With the use of the normalizing values,  $\rho_0$  and  $N_0$ , the magnitude of  $X$  is almost always less than 4. This is desirable from a computational standpoint because the computation is much less sensitive to the number of significant figures retained in the coefficients.

The data used for the curve fitting consisted of 26 points obtained from the C-V measurements, 12 points determined from the Hall effect measurements, 2 points from Esaki and Miyahara [43], and 1 point from Fair and Tsai [35]. The latter three points are listed in table 8 and were included to increase

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\* A value of  $1.602 \times 10^{-19} \text{ C}$  was used for  $q$  in all of the curve fits; consequently, this is the appropriate value to use for subsequent calculations.

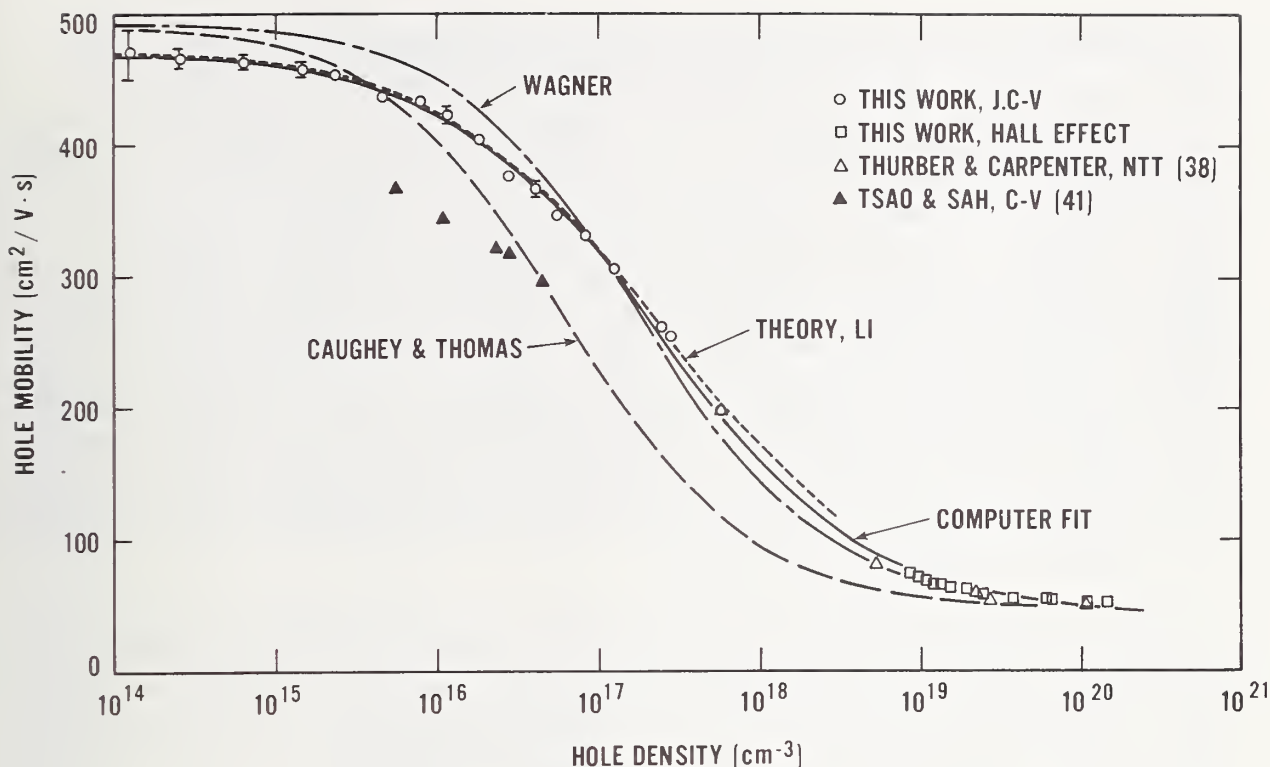


Figure 8. Hole mobility as a function of calculated hole density for boron-doped silicon at 300 K. All data points, except those in the heavily doped range, have been corrected for incomplete ionization using the work of Li [37]. The Caughey-Thomas [1] and Wagner [4] expressions were obtained without consideration of de-ionization and are plotted assuming equivalence of hole and dopant densities. This gives lower mobility in the range  $10^{17}$  to  $10^{19}$   $\text{cm}^{-3}$ . The error bars on the C-V data of this work show the standard deviation calculated from the individual mobility values for that wafer. When not shown, the error bars lie within the plotted symbol.

Table 8. Miscellaneous Data for the Computer Curve Fits of Phosphorus-Doped Silicon.

| Point No. | Source                     | N<br>$\text{cm}^{-3}$       | $\rho_{23^\circ\text{C}}$<br>$\Omega \cdot \text{cm}$ | $\rho_{300\text{ K}}$<br>$\Omega \cdot \text{cm}$ | n<br>$\text{cm}^{-3}$ | $\mu_{23^\circ\text{C}}$<br>$\text{cm}^2/\text{V} \cdot \text{s}$ | $\mu_{300\text{ K}}$<br>$\text{cm}^2/\text{V} \cdot \text{s}$ |
|-----------|----------------------------|-----------------------------|---|---|-----------------------|---|---|
| 1         | experimental extrapolation | $1 \times 10^{12}$          | 4276.0  | 4413.0  | $1 \times 10^{12}$    | 1460  | 1415  |
| 2         | NAA/photometric            | $1.25 \times 10^{18}$       | 0.020   | 0.020   | $1.13 \times 10^{18}$ | 276   | 276   |
| 3         | NAA/photometric            | $2.57 \times 10^{18}$       | 0.014   | 0.014   | $2.23 \times 10^{18}$ | 200   | 200   |
| 4         | NAA/photometric            | $4.70 \times 10^{18}$       | 0.010   | 0.010   | $4.70 \times 10^{18}$ | 133   | 133   |
| 5         | NAA/photometric            | $7.75 \times 10^{18}$       | 0.0073  | 0.0073  | $7.75 \times 10^{18}$ | 110   | 110   |
| 6         | Esaki & Miyahara [43]      | $1.2 \times 10^{20\dagger}$ | 0.00067   | 0.00067   | $1.2 \times 10^{20}$  | 78  | 78  |
| 7         | Esaki & Miyahara [43]      | $1.6 \times 10^{20\dagger}$ | 0.00055   | 0.00055   | $1.6 \times 10^{20}$  | 71  | 71  |
| 8         | Fair & Tsai [35]           | $3 \times 10^{20\dagger}$   | 0.000298  | 0.000298  | $3 \times 10^{20}$    | *   | *   |

<sup>†</sup>Electrically active dopant density assumed equal to electron density.

\*Not included in mobility fit.

the range of the fit at high densities beyond that justified by the data of this work alone. In the region of the gap between the C-V and Hall effect data (phosphorus densities between  $10^{18}$  and  $10^{19}$   $\text{cm}^{-3}$ ), four resistivity-dopant density pairs were generated for the data base to be used in the curve fitting. These pairs, listed in table 8, were based on the NAA and photometric results, but actual values were chosen to give a smooth curve between the C-V and Hall effect data. In addition, a point was added at  $N = 1 \times 10^{12}$   $\text{cm}^{-3}$  to improve the fit for calculating values in the low dopant density range. This point was taken equal to the average of the four lowest dopant density data points since the  $\rho N$  product is essentially constant in this region. Also, the inclusion of this point helps insure that the fits as a function of  $\log_{10} (\rho/\rho_0)$  and  $\log_{10} (N/N_0)$  both give essentially the same calculated values in this region. The coefficients for the fit of the data to eq (1) are given in table 9 for 23°C and 300 K. The table gives the approximate standard deviation for each coefficient and the residual standard deviation (R.S.D.) in units of volts-second per square centimeter. The R.S.D. is the square root of the quotient of the sum of the squared residuals,\* divided by the number of degrees of freedom.

The plot of the data used for the curve fit, with the exception of the point at  $10^{12}$   $\text{cm}^{-3}$ , and the least squares fit of the  $q\rho N$  product *versus*  $N$  for 300 K are shown in figure 9. This figure clearly shows that the "min-max" expressions of Caughey and Thomas [1] are not suitable for these data as there is no plateau or maximum at high dopant densities. The curve obtained for the product as a function of resistivity is plotted in figure 10.

The two expressions, one a function of  $\log_{10} (\rho/\rho_0)$  and the other a function of  $\log_{10} (N/N_0)$ , have a worst case self-consistency of 8 percent for all values of  $N$  (and corresponding values of  $\rho$ ) within the range  $1 \times 10^{12}$  to  $4 \times 10^{20}$   $\text{cm}^{-3}$ . That is, when the product  $q\rho N$  is calculated for a given  $N$ , giving a  $\rho$  which is used in the  $q\rho N$  *versus*  $\rho$  expression to again calculate the product, the latter product will be within 8 percent of the former. The maximum difference occurs only in the low  $10^{18}$   $\text{cm}^{-3}$  range; elsewhere the fits are consistent within 4 percent. When the self-consistency is calculated starting with a given  $\rho$ , the fits have a maximum difference of 4 percent for resistivities from  $2 \times 10^{-4}$  to  $3 \times 10^3$   $\Omega \cdot \text{cm}$ . The self-consistency is shown (solid curves) as a function of dopant density in figure 11 and as a function of resistivity in figure 12.

Curve fits were also obtained for electron mobility as a function of both electron density,  $n$ , and resistivity. It was found that better and more self-consistent fits were possible if the point at  $3 \times 10^{20}$   $\text{cm}^{-3}$  were omitted. Otherwise the data used for the mobility fits corresponded to that used for the product fits. As mentioned previously, the percent ionization calculations of Li and Thurber [30] were used to obtain the electron density from the measured dopant density prior to the computation of mobility. The expression for calculating the electron mobility is of the form

$$\log_{10} (\mu/\mu_0) = \frac{A_0 + A_1 X + A_2 X^2 + A_3 X^3}{1 + B_1 X + B_2 X^2 + B_3 X^3}, \quad (2)$$

\* The difference between the measured point and the predicted value from the curve fit.

Table 9. Coefficients and Residual Standard Deviation (R.S.D.) for the Fit of the Product  $q\rho N$  for Phosphorus-Doped Silicon Using Eq (1).

| Temp.<br>X     | 23°C<br>$\log_{10} (\rho/\rho_0)$ | 23°C<br>$\log_{10} (N/N_0)$ | 300 K<br>$\log_{10} (\rho/\rho_0)$ | 300 K<br>$\log_{10} (N/N_0)$ |
|----------------|-----------------------------------|-----------------------------|------------------------------------|------------------------------|
| A <sub>0</sub> | -3.1083 ± 0.0038                  | -3.0769 ± 0.0027            | -3.0951 ± 0.0037                   | -3.0652 ± 0.0026             |
| A <sub>1</sub> | -3.2626 ± 0.0952                  | 2.2108 ± 0.0392             | -3.2303 ± 0.0909                   | 2.1853 ± 0.0415              |
| A <sub>2</sub> | -1.2196 ± 0.0341                  | -0.62272 ± 0.0159           | -1.2024 ± 0.0325                   | -0.61080 ± 0.0170            |
| A <sub>3</sub> | -0.13923 ± 0.00468                | 0.057501 ± 0.00287          | -0.13679 ± 0.00466                 | 0.056189 ± 0.00327           |
| B <sub>1</sub> | 1.0265 ± 0.0318                   | -0.68157 ± 0.0134           | 1.0205 ± 0.0305                    | -0.67642 ± 0.0141            |
| B <sub>2</sub> | 0.38755 ± 0.0109                  | 0.19833 ± 0.00507           | 0.38382 ± 0.0105                   | 0.19542 ± 0.00541            |
| B <sub>3</sub> | 0.041833 ± 0.00168                | -0.018376 ± 0.000986        | 0.041338 ± 0.00169                 | -0.018100 ± 0.00112          |
| R.S.D.         | 2.78 × 10 <sup>-4</sup>           | 2.21 × 10 <sup>-4</sup>     | 2.67 × 10 <sup>-4</sup>            | 2.09 × 10 <sup>-4</sup>      |

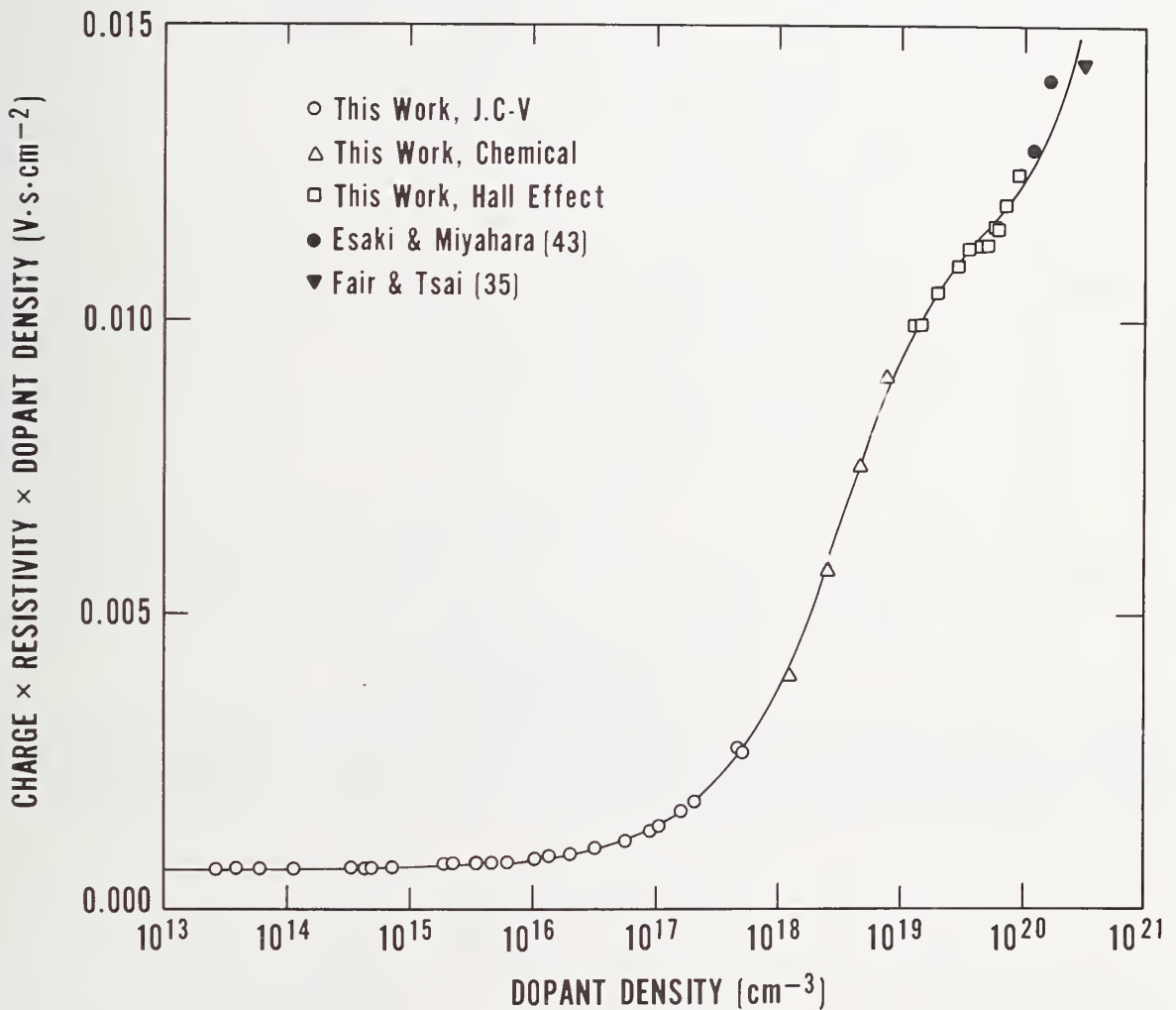


Figure 9. The  $q\rho N$  product as a function of dopant density for phosphorus-doped silicon at 300 K. The curve is the least squares fit to the data points shown using eq (1). Coefficients are given in table 9.

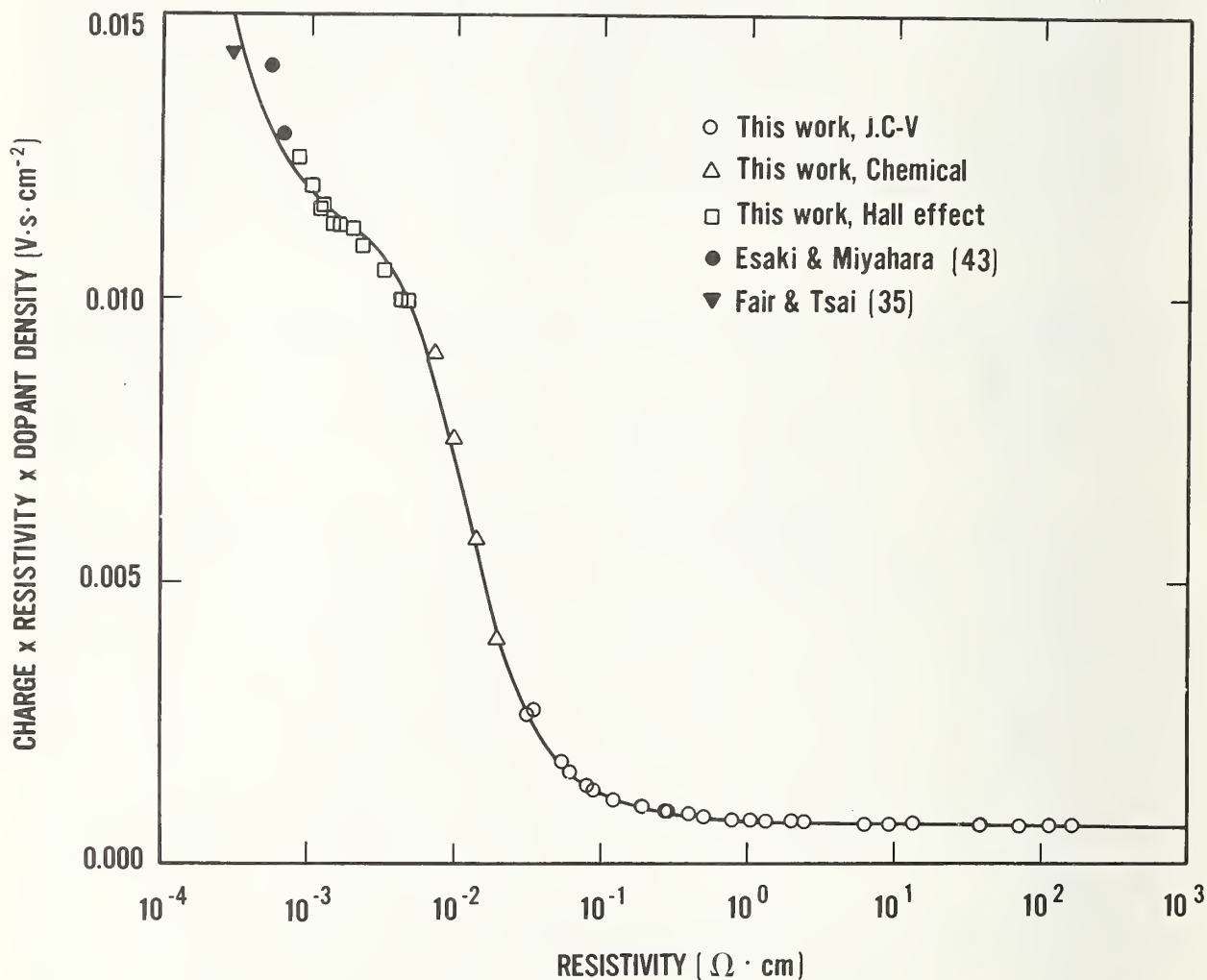


Figure 10. The  $q\rho N$  product as a function of resistivity for phosphorus-doped silicon at 300 K. Equation (1) was used as the form of the curve fit to the data points shown. Coefficients are given in table 9.

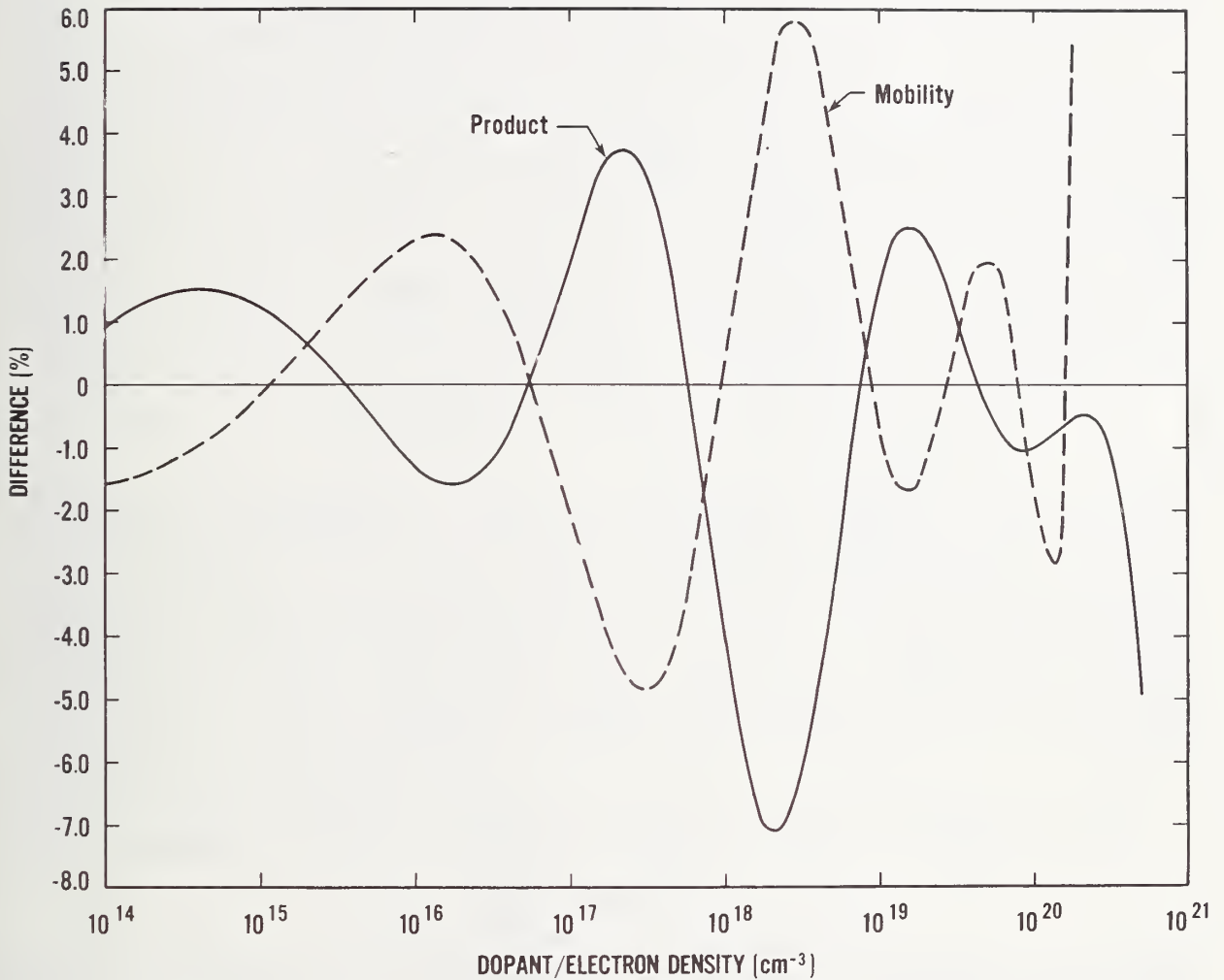


Figure 11. Self-consistency of the product and mobility fits at 23°C for phosphorus-doped silicon plotted *versus* dopant density for the product fits and *versus* electron density for the mobility fits. The procedure for calculating the difference is discussed in the text.

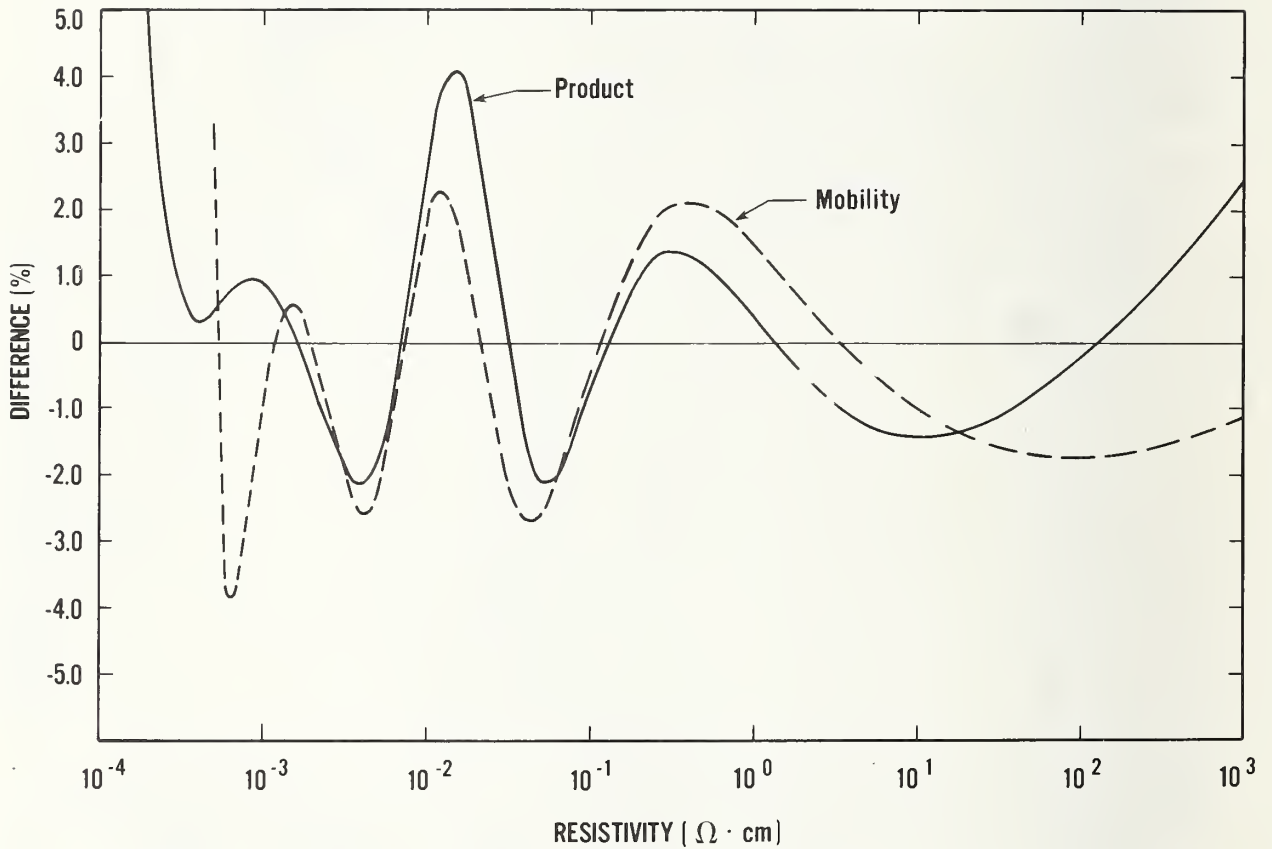


Figure 12. Self-consistency of the product and mobility fits at 23°C for phosphorus-doped silicon plotted *versus* resistivity. The procedure for calculating the difference is discussed in the text.



where  $\mu$  is the mobility and  $\mu_0 = 1 \text{ cm}^2/\text{V}\cdot\text{s}$ . (In this equation, the A's and B's represent coefficients to be determined; they are not constants from previous fits.) As before, fits were made for both  $X = \log_{10} (\rho/\rho_0)$  and  $X = \log_{10} (n/n_0)$  for temperatures of 23°C and 300 K. Values for the coefficients are given in table 10. The plot of the mobility data and fitted curve as a function of resistivity for 300 K is given in figure 13. The fit of mobility *versus* electron density is shown in figures 5 and 6 for comparison with experimental data. An expression of the form suggested by Masetti and Solmi [36] was also tried for the mobility fits, but the percent residuals in the low mobility range were significantly larger than with eq (2), particularly for the fit as a function of resistivity.

The self-consistency of the mobility fits, plotted as dashed curves in figures 11 and 12, shows a maximum difference of 6 percent for electron densities in the range  $10^{12}$  to  $10^{20} \text{ cm}^{-3}$ . The expressions rapidly diverge for densities greater than  $2 \times 10^{20} \text{ cm}^{-3}$ . The fit as a function of resistivity is the better choice for approximating mobility values beyond the range of the fitted data. When the self-consistency is calculated starting with a given resistivity, the fits have a maximum difference of 3 percent for resistivities from  $6 \times 10^{-4}$  to  $10^4 \Omega\cdot\text{cm}$ . The self-consistency graphs shown are for 23°C; calculations for 300 K closely parallel those for 23°C.

## 8. COMPUTER CURVE FITS FOR BORON-DOPED SILICON

The previous expressions for the fits to phosphorus-doped silicon are in the form of quotients of two third-degree polynomials in order to fit the shape of the product and mobility curves at high phosphorus densities. However, for boron-doped silicon, the product is well behaved at very high densities, such that "min-max" relationships similar to those proposed by Caughey and Thomas [1] give satisfactory fits. Modifications are necessary for the fits of mobility as will be discussed later. These relationships have the advantage that two of the parameters,  $(q\rho N)_{\min}$  and  $(q\rho N)_{\max}$ , have a readily identified physical significance in that they approximately equal the true limiting value of these quantities.

The expression for the product  $q\rho N$  as a function of  $\rho$  was taken as

$$q\rho N = (q\rho N)_{\min} + \frac{(q\rho N)_{\max} - (q\rho N)_{\min}}{1 + \left(\frac{\rho}{\rho_{\text{ref}}}\right)^\alpha}, \quad (3)$$

where  $q$  is the electronic charge,  $N$  is the boron density,  $\rho$  is the resistivity,  $(q\rho N)_{\min}$  and  $(q\rho N)_{\max}$  are the asymptotic minimum and maximum values of the product,  $\rho_{\text{ref}}$  is a reference value corresponding to the resistivity for which the derivative of the product is a maximum, and  $\alpha$  is a measure of the slope of the curve near the reference value. The data used for the fit, given in tables 5, 6, and 7, were the junction C-V and Hall effect results of this work, and selected NTT results for boron densities greater than  $5 \times 10^{17} \text{ cm}^{-3}$ . The NTT data at lower densities were omitted because the data, while in general agreement with the C-V results, showed significantly more scatter. For high boron densities, the NTT results may be better than those from the Hall effect because of the need to assume a value for the Hall

Table 10. Coefficients and Residual Standard Deviation (R.S.D.) for the Fit of Electron Mobility for Phosphorus-Doped Silicon Using Eq (2).

| Temp.<br>X     | 23°C<br>$\log_{10} (\rho/\rho_0)$ | 23°C<br>$\log_{10} (n/n_0)$ | 300 K<br>$\log_{10} (\rho/\rho_0)$ | 300 K<br>$\log_{10} (n/n_0)$ |
|----------------|-----------------------------------|-----------------------------|------------------------------------|------------------------------|
| A <sub>0</sub> | 3.1122 ± 0.0034                   | 3.0746 ± 0.0025             | 3.0985 ± 0.0037                    | 3.0629 ± 0.0025              |
| A <sub>1</sub> | 3.3347 ± 0.0951                   | -2.2679 ± 0.0076            | 3.3257 ± 0.0923                    | -2.2522 ± 0.0077             |
| A <sub>2</sub> | 1.2610 ± 0.0511                   | 0.62998 ± 0.00245           | 1.2581 ± 0.0481                    | 0.62327 ± 0.00249            |
| A <sub>3</sub> | 0.15701 ± 0.0198                  | -0.061285 ± 0.00087         | 0.15679 ± 0.0189                   | -0.060415 ± 0.00087          |
| B <sub>1</sub> | 1.0463 ± 0.0324                   | -0.70017 ± 0.00290          | 1.0485 ± 0.0317                    | -0.69851 ± 0.00292           |
| B <sub>2</sub> | 0.39941 ± 0.0167                  | 0.19839 ± 0.00113           | 0.40020 ± 0.0156                   | 0.19716 ± 0.00114            |
| B <sub>3</sub> | 0.049746 ± 0.00547                | -0.020150 ± 0.00041         | 0.049883 ± 0.00512                 | -0.019950 ± 0.00041          |
| R.S.D.         | 14.9                              | 11.6                        | 14.8                               | 11.2                         |

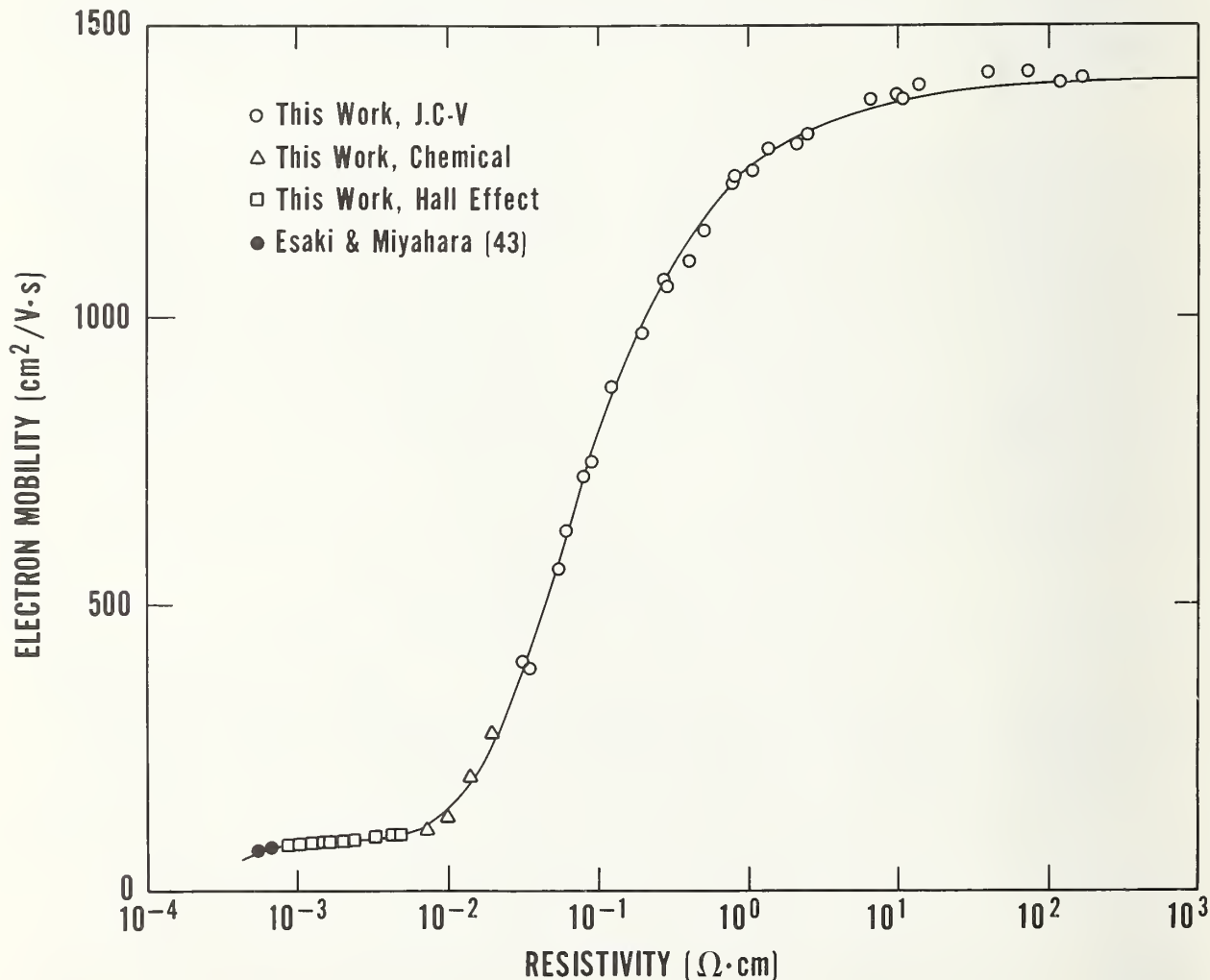


Figure 13. Electron mobility *versus* resistivity at 300 K for phosphorus-doped silicon. The curve is the least squares fit to the points using eq (2) with coefficients given in table 10.

factor in the latter case. This same set of 300 K data, and its counterpart at 23°C, was used for all of the curve fits. The resistivity values of the 39 fitted data points spanned the range 0.00085 to 100  $\Omega \cdot \text{cm}$  with corresponding dopant densities between  $1.4 \times 10^{20}$  and  $1.3 \times 10^{14} \text{ cm}^{-3}$ . The least-squares curve at 300 K is shown in figure 8 for comparison with experimental data and other curves. All four parameters as determined by the fit are given in table 11 for both 23°C and 300 K. The approximate standard deviation is given for each parameter in its own units, and the residual standard deviation (R.S.D.) for the fit is listed in units of  $q\rho N$ .

The expression for the product  $q\rho N$  as a function of dopant density has the same form as eq (3) except for a negative value of the exponent because of the inverse relationship between  $\rho$  and  $N$ :

$$q\rho N = (q\rho N)_{\min} + \frac{(q\rho N)_{\max} - (q\rho N)_{\min}}{1 + \left(\frac{N}{N_{\text{ref}}}\right)^{\alpha}} \quad (4)$$

(In this equation  $(q\rho N)_{\min}$ ,  $(q\rho N)_{\max}$ ,  $N_{\text{ref}}$ , and  $\alpha$  represent the parameters to be determined; they are not constants from previous fits.) Values for the four parameters are listed in table 12 for both 23°C and 300 K. The curve for 300 K and the experimental data used to obtain it are shown in figure 14.

In comparing the product fits as a function of resistivity with those as a function of dopant density, it is evident that minimum and maximum values which should be correspondingly equal are somewhat different. This is, of course, a consequence of the independent fits where no parameters are fixed. The  $(q\rho N)_{\min}$  values differ by 2 percent and the fits differ by this same percentage at  $N = 10^{14} \text{ cm}^{-3}$ . The  $(q\rho N)_{\max}$  values differ by 4 percent; however, these are asymptotic values, and at the upper limit of the experimental data ( $N \approx 10^{20} \text{ cm}^{-3}$ ) there is still considerable curvature. The difference between the fits in this region is less than 1 percent. The product fits are self-consistent within 3 percent for all dopant densities (and corresponding resistivities) in the range  $10^{14}$  to  $10^{20} \text{ cm}^{-3}$ ; see the solid curves in figures 15 and 16. That is, when the product  $q\rho N$  is calculated for a given dopant density with eq (4), a resistivity is derived which can be used in the  $q\rho N$  versus  $\rho$  expression [eq (3)] to again calculate the product. The latter product will be within 3 percent of the former.

Hole mobilities were calculated from resistivity and hole density values. Except in the heavily doped range, where hole density is assumed to equal dopant density, hole densities were obtained from dopant densities using the percent ionization calculations of Li [37]. A suitable expression for the hole mobility,  $\mu_h$ , as a function of hole density,  $p$ , was found to be

$$\mu_h = A \exp(-p_c/p) + \frac{\mu_{\max}}{1 + \left(\frac{p}{p_{\text{ref}}}\right)^{\alpha}} \quad (5)$$

This form gave a significantly better fit than the simpler form of the type used for fitting the product curves. The effect of the exponential factor in

Table 11 – Parameters and Residual Standard Deviation (R.S.D.) for the Fit of  $q\rho N$  versus  $\rho$  for Boron-Doped Silicon Using Eq (3).

| Temperature                              | 23°C                  | 300 K                 |
|--|-----------------------|-----------------------|
| $(q\rho N)_{\min}$ ( $V\cdot s/cm^2$ )   | 0.00213 $\pm$ 0.00009 | 0.00220 $\pm$ 0.00009 |
| $(q\rho N)_{\max}$ ( $V\cdot s/cm^2$ )   | 0.01947 $\pm$ 0.00018 | 0.01973 $\pm$ 0.00017 |
| $\rho_{\text{ref}}$ ( $\Omega\cdot cm$ ) | 0.01833 $\pm$ 0.00067 | 0.01782 $\pm$ 0.00060 |
| $\alpha$                                 | 1.105 $\pm$ 0.035     | 1.086 $\pm$ 0.032     |
| R.S.D. ( $V\cdot s/cm^2$ )               | 0.000292              | 0.000266              |

Table 12 – parameters and Residual Standard Deviation (R.S.D.) for the Fit of  $q\rho N$  versus  $N$  for Boron-Doped Silicon Using Eq (4).

| Temperature                            | 23°C  | 300 K   |
|--|---|---|
| $(q\rho N)_{\min}$ ( $V\cdot s/cm^2$ ) | 0.00209 $\pm$ 0.00009                             | 0.00215 $\pm$ 0.00008                             |
| $(q\rho N)_{\max}$ ( $V\cdot s/cm^2$ ) | 0.02024 $\pm$ 0.00024                             | 0.02053 $\pm$ 0.00022                             |
| $N_{\text{ref}}$ ( $cm^{-3}$ )         | $3.88 \times 10^{18}$ $\pm$ $0.21 \times 10^{18}$ | $4.09 \times 10^{18}$ $\pm$ $0.20 \times 10^{18}$ |
| $\alpha$                               | -0.737 $\pm$ 0.024                                | -0.727 $\pm$ 0.021                                |
| R.S.D. ( $V\cdot s/cm^2$ )             | 0.000268  | 0.000240  |

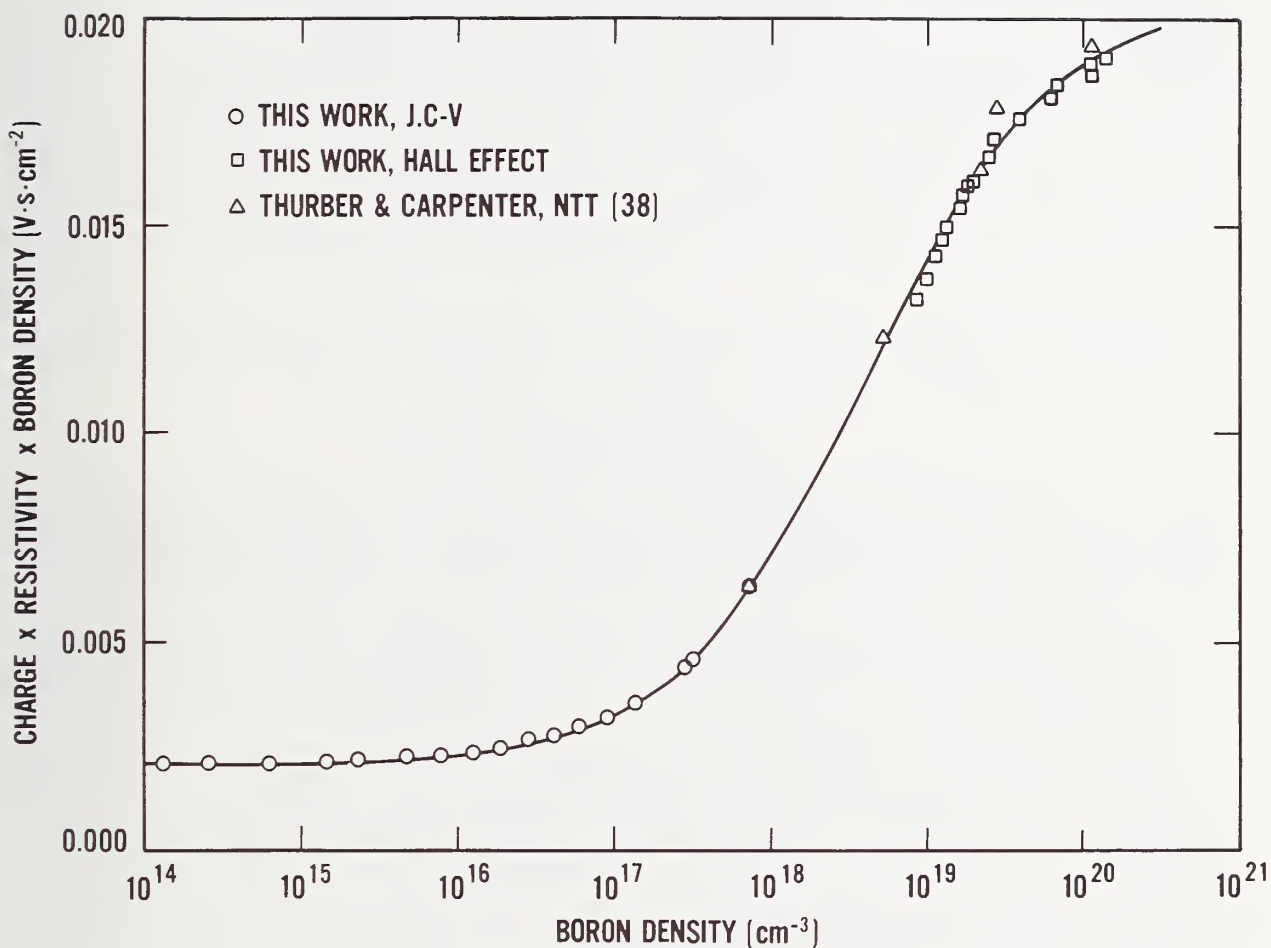


Figure 14. The  $q\rho l$  product as a function of boron density for 300 K. The curve is an analytical fit to the data points shown using eq (4). Parameter values are given in table 12.

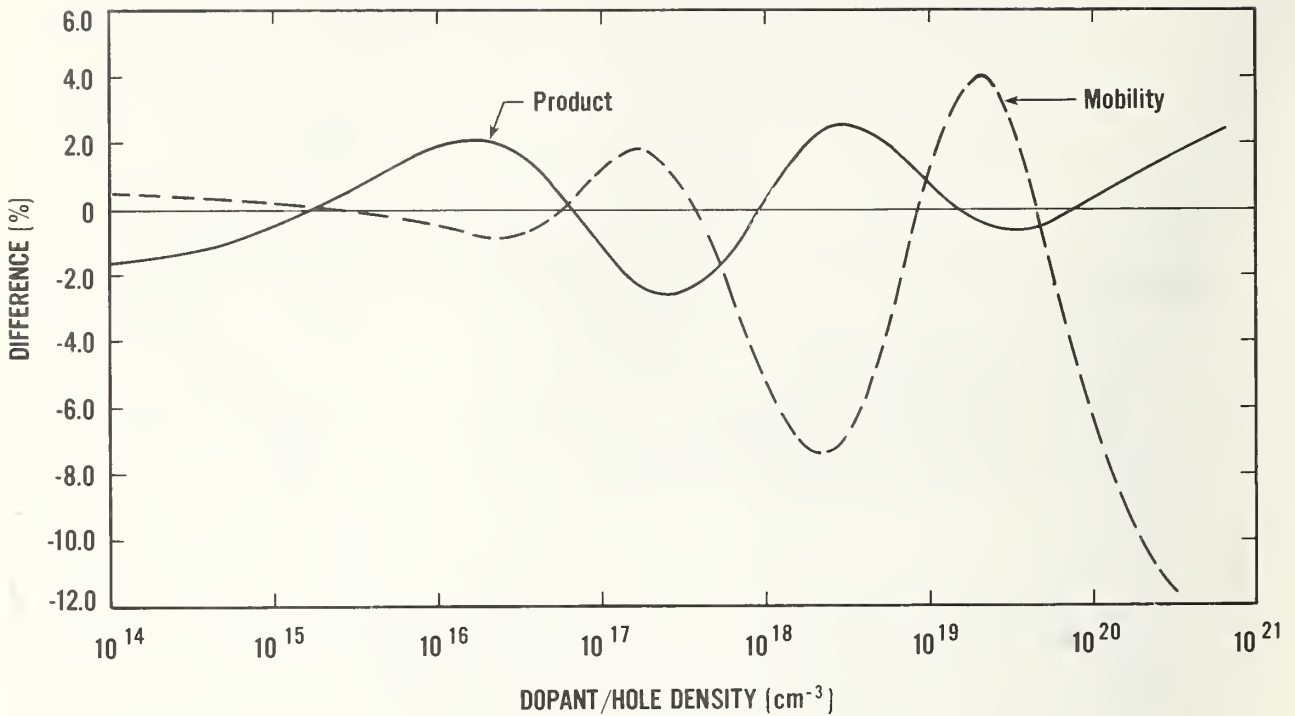


Figure 15. Self-consistency of the product and mobility fits at 23°C for boron-doped silicon plotted *versus* dopant density for the product fits and *versus* hole density for the mobility fits. The procedure for calculating the difference is discussed in the text.

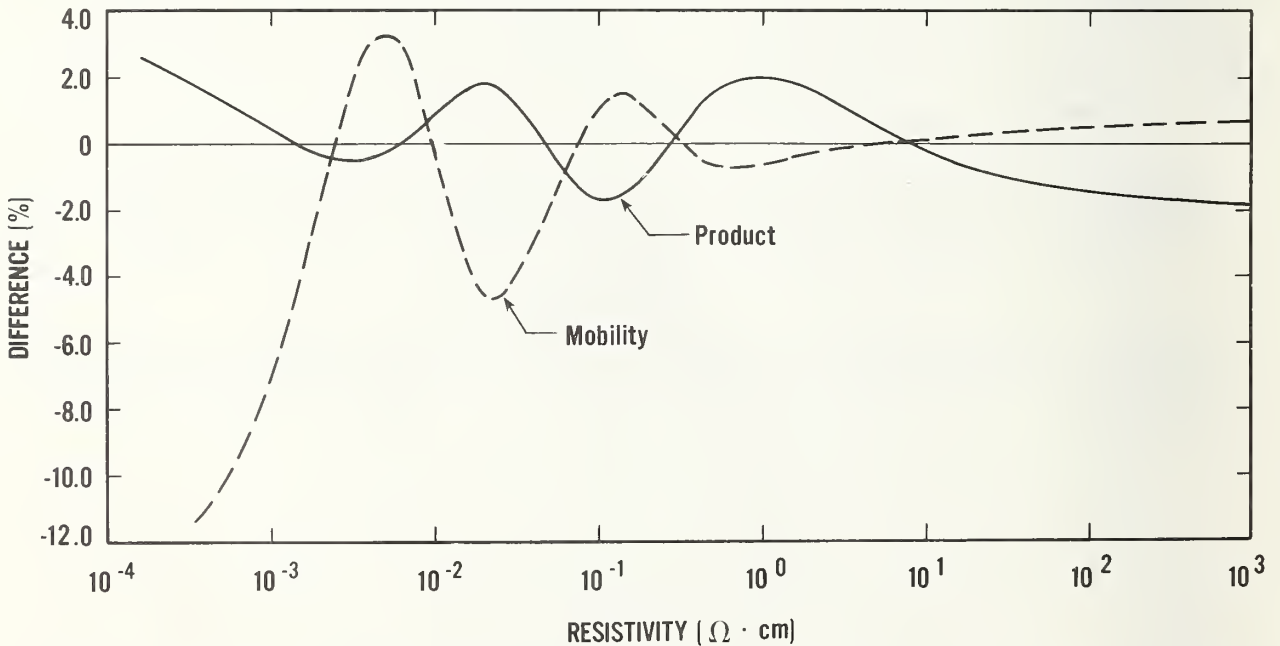


Figure 16. Self-consistency of the product and mobility fits at 23°C for boron-doped silicon plotted *versus* resistivity. The procedure for calculating the difference is discussed in the text.

the first term is to increase the mobility in the region of the curve where the dopant and hole densities deviate significantly from each other. The hole mobility approaches the constant value A for very large hole densities. The five parameters, determined by the fit to the 39 data points, are listed in table 13 for 23°C and 300 K. The curve for 300 K, calculated using the parameters in table 13, is shown in figure 8 for comparison with experimental data and other curves.

During the course of fitting the hole mobility to eq (5), it was found that convergence was obtained for two different values of  $p_c$ . Further work confirmed that there were two valleys, or local minima, for the variation of the R.S.D. with  $p_c$ , and the one located by the fitting procedure depended on the starting value for  $p_c$ . At 23°C one fit had  $p_c = 9.00 \times 10^{16}$ ,  $A = 45.2$ ,  $\mu_{max} = 486.1$ ,  $p_{ref} = 2.11 \times 10^{17}$ ,  $\alpha = 0.718$ , and R.S.D. = 3.18; the other had  $p_c = 1.09 \times 10^{19}$ ,  $A = 41.4$ ,  $\mu_{max} = 492.5$ ,  $p_{ref} = 3.06 \times 10^{17}$ ,  $\alpha = 0.589$ , and R.S.D. = 2.84. The former fit was selected in spite of its higher R.S.D. because it gave better self-consistency with the fit as a function of resistivity.

The form for the hole mobility as a function of resistivity was taken as

$$\mu_h = A \exp(-\rho/\rho_c) + \frac{\mu_{max}}{1 + \left(\frac{\rho}{\rho_{ref}}\right)^\alpha} \quad (6)$$

It was also found that the simple "min-max" form did not fit the mobility *versus* resistivity data well, particularly in the low resistivity range. The inclusion of the exponential in the first term improved the fit considerably. Its effect is similar to that of the exponential in eq (5). In this expression, the mobility is dominated by the first term at low resistivities and by the second term at high resistivities. The parameters determined by the fit are listed in table 14 for both 23°C and 300 K. The curve for 300 K and the experimental data used for the fit are shown in figure 17. The curve fits the shape of the experimental data very well at low resistivities so that extrapolation of eq (6), using the parameters in table 14, at the low resistivity end should give reasonable values. Thus, A can be considered to be approximately equal to the minimum value of the mobility. The mobility *versus* hole density fit is not as good at the low mobility end, as it is slightly below the data at  $p = 10^{20} \text{ cm}^{-3}$  and goes to a lower asymptotic value than is the case for eq (6). Consequently, an extrapolation of eq (5) at the low mobility end is less likely to be correct.

The  $\mu_{max}$  values for the mobility fits as a function of hole density differ by about 0.7 percent from the  $\mu_{max}$  values for the fits as a function of resistivity. The mobility fits are self-consistent within 2 percent for all hole densities (and corresponding resistivities) in the range  $10^{14}$  to  $5 \times 10^{17} \text{ cm}^{-3}$ ; see the dashed curves in figures 15 and 16. In the  $10^{18} \text{ cm}^{-3}$  range, there are differences of up to 8 percent. The self-consistency improves in the low  $10^{19} \text{ cm}^{-3}$  range but increases again to 6 percent at  $10^{20} \text{ cm}^{-3}$  as the fits depart for very heavy doping.

The results of this work are incorporated in the ASTM document F 723 entitled "Practice for the Conversion Between Resistivity and Dopant Density for

Table 13 – Parameters and Residual Standard Deviation (R.S.D.) for the Fit of  $\mu_h$  versus  $p$  Using Eq (5).

| Temperature                        | 23°C                    |                           | 300 K                   |                           |
|------------------------------------|-------------------------|---------------------------|-------------------------|---------------------------|
| A (cm <sup>2</sup> /V·s)           | 45.2                    | ± 1.3                     | 44.9                    | ± 1.2                     |
| $p_c$ (cm <sup>-3</sup> )          | 9.00 x 10 <sup>16</sup> | ± 2.3 x 10 <sup>16</sup>  | 9.23 x 10 <sup>16</sup> | ± 2.3 x 10 <sup>16</sup>  |
| $\mu_{max}$ (cm <sup>2</sup> /V·s) | 486.1                   | ± 1.9                     | 470.5                   | ± 1.8                     |
| $p_{ref}$ (cm <sup>-3</sup> )      | 2.11 x 10 <sup>17</sup> | ± 0.09 x 10 <sup>17</sup> | 2.23 x 10 <sup>17</sup> | ± 0.10 x 10 <sup>17</sup> |
| $\alpha$                           | 0.718                   | ± 0.013                   | 0.719                   | ± 0.013                   |
| R.S.D. (cm <sup>2</sup> /V·s)      | 3.18                    |                           | 3.07                    |                           |

Table 14 – Parameters and Residual Standard Deviation (R.S.D.) for the Fit of  $\mu_h$  versus  $\rho$  Using Eq (6).

| Temperature                               | 23°C    |           | 300 K   |           |
|---|---------|-----------|---------|-----------|
| A (cm <sup>2</sup> /V·s)                  | 52.4    | ± 3.8     | 51.6    | ± 3.7     |
| $\rho_c$ ( $\Omega \cdot \text{cm}$ )     | 0.00409 | ± 0.00077 | 0.00406 | ± 0.00077 |
| $\mu_{max}$ (cm <sup>2</sup> /V·s)        | 482.8   | ± 2.4     | 467.3   | ± 2.4     |
| $\rho_{ref}$ ( $\Omega \cdot \text{cm}$ ) | 0.0825  | ± 0.0020  | 0.0794  | ± 0.0019  |
| $\alpha$                                  | -0.811  | ± 0.018   | -0.808  | ± 0.019   |
| R.S.D. (cm <sup>2</sup> /V·s)             | 4.89    |           | 4.78    |           |



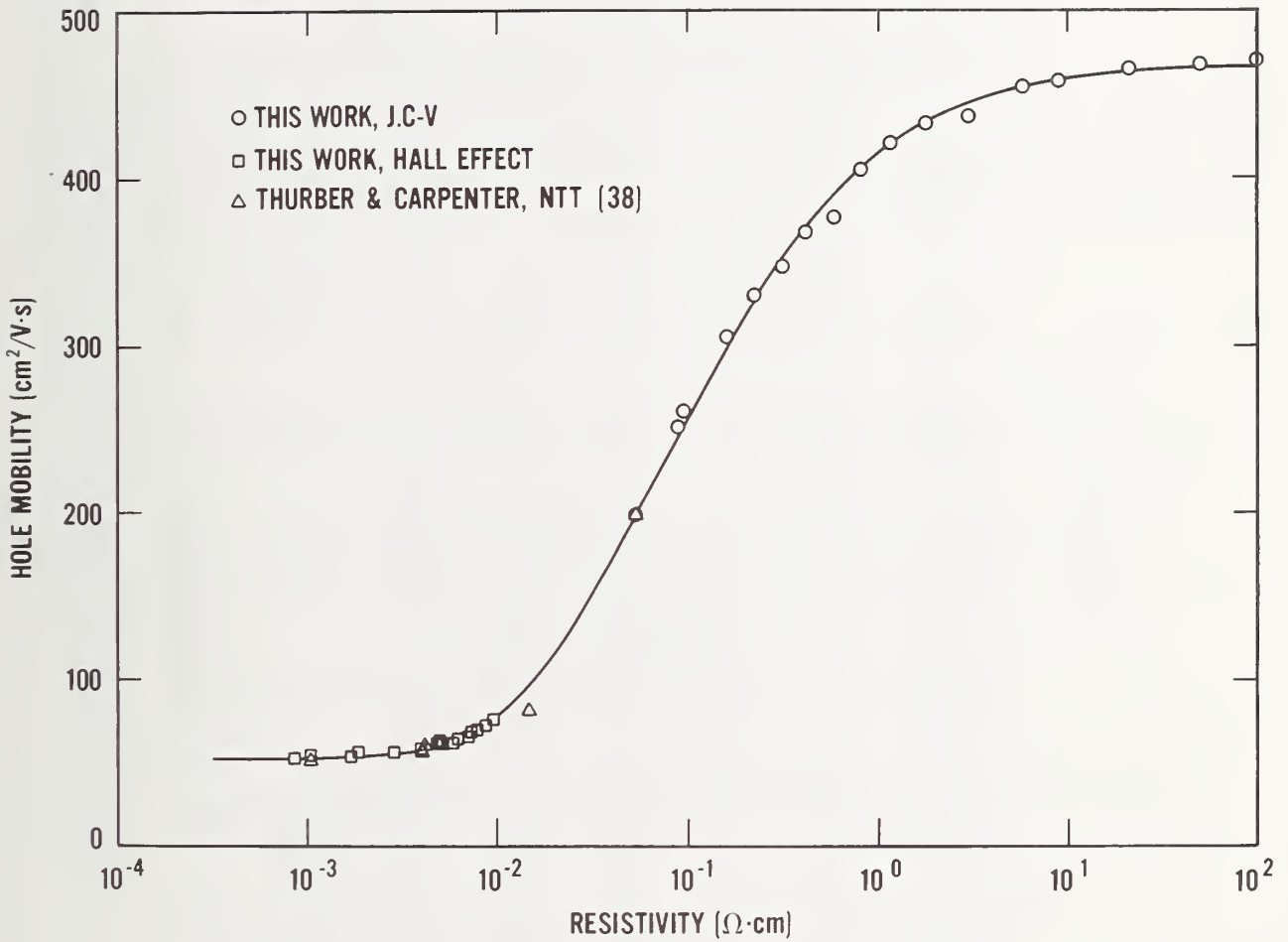


Figure 17. Hole mobility *versus* resistivity at 300 K for boron-doped silicon. The curve is an analytical fit to the data points shown using eq (6). Parameter values are given in table 14.

## CONVERSION BETWEEN RESISTIVITY AND DOPANT DENSITY

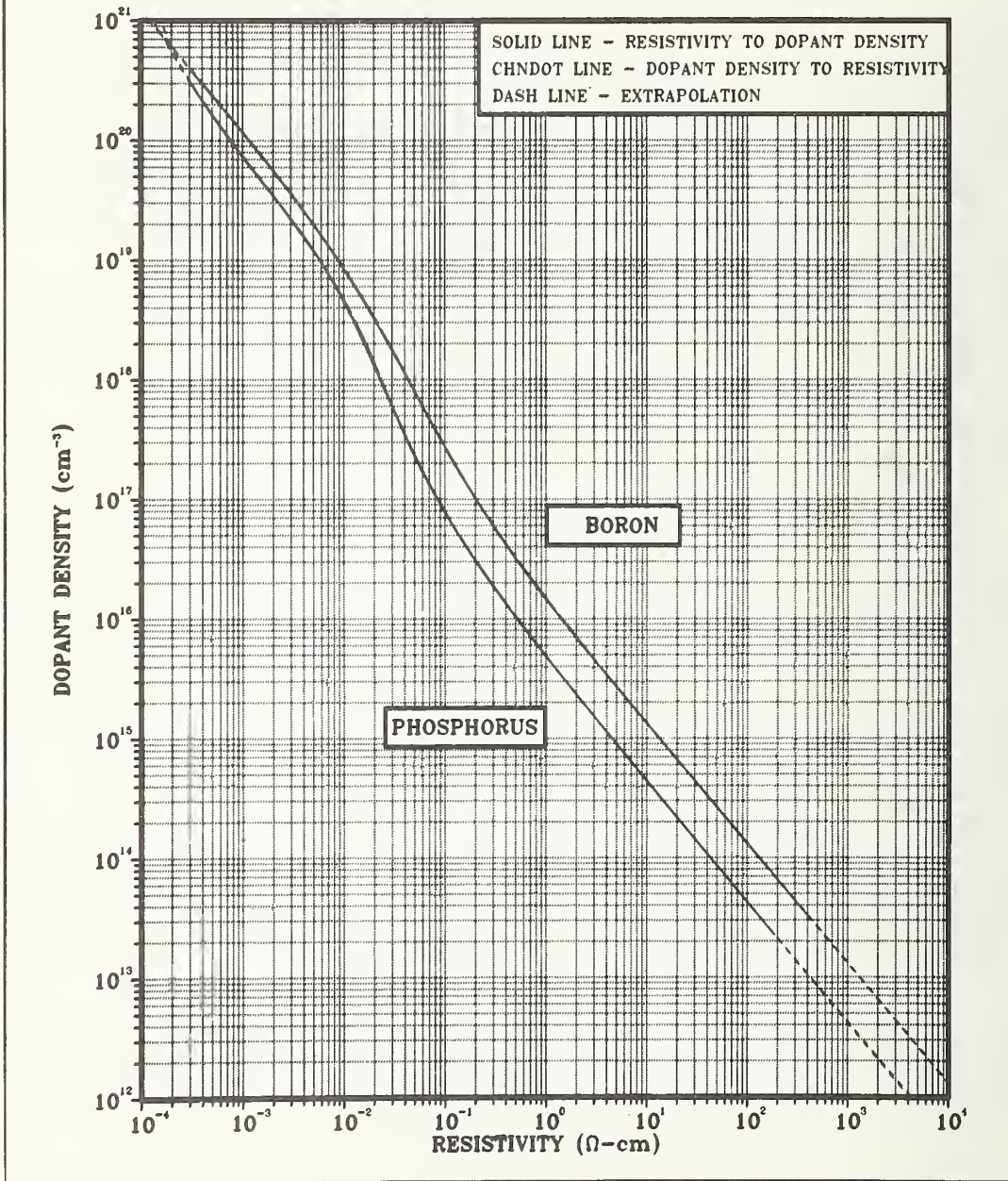


Figure 18. Dopant density *versus* resistivity at 23°C for silicon doped with phosphorus and with boron. The solid line shows the dopant density calculated from the equation of the product as a function of resistivity for the region of actual data. The chain-dot line shows the resistivity calculated from the equation of the product as a function of dopant density for the region of actual data. Dashed lines show the extrapolation beyond the region covered by the data. On the scale of the figure shown here, the solid and chain-dot lines are indistinguishable. However, in regions where the self-consistency error is appreciable, the lines are distinguishable on the wall chart available from ASTM. (Graph is from ASTM document F 723 cited in the text.)

Boron- and Phosphorus-Doped Silicon" which has been approved by Committee F-1 on Electronics and will appear in the 1981 Annual Book of ASTM Standards, Part 43. This document provides three procedures for converting between resistivity and dopant density at 23°C. They are: (1) graphical method - a graph, reproduced as figure 18 of this report, with curves for both boron and phosphorus; (2) tabular method - a set of four tables covering the two dopants as functions of both resistivity and dopant density; and (3) computational method - the same equations and coefficients as given in this report for use when exact calculations are most convenient or necessary. The document does not cover electron or hole mobility relationships.

## 9. CONCLUSIONS

For phosphorus-doped silicon, the relationship between resistivity and dopant density was determined for densities between  $10^{13}$  and  $10^{20}$   $\text{cm}^{-3}$ . The results differ from the *n*-type Irvin curve by 5 to 15 percent, always in the direction of lower resistivity for a given dopant density. The work is in agreement with that of Mousty *et al.* in the  $10^{15}$  to  $10^{18}$   $\text{cm}^{-3}$  range, but differences exist for lower and for higher doping levels.

For boron-doped silicon resistivity and dopant density data were obtained for boron densities between  $10^{14}$  and  $10^{20}$   $\text{cm}^{-3}$ . The results differ significantly from the commonly used Irvin curve for densities greater than  $10^{16}$   $\text{cm}^{-3}$  with a maximum deviation of 45 percent at  $5 \times 10^{17}$   $\text{cm}^{-3}$  in the direction of lower resistivity for a given boron density. Hole mobility values, calculated from this work with correction for percent ionization of the dopant atoms, are much larger than the experimental data of Tsao and Sah, but are in good agreement with the theoretical calculations of Li. The hole mobility values are in reasonable agreement with Wagner's work on boron-implanted silicon. The maximum discrepancy occurs in the  $10^{18}$   $\text{cm}^{-3}$  range where the Wagner mobility is 10 percent lower because deionization effects were not included.

Analytical expressions, convenient for engineering calculations, were fitted to the resistivity-dopant density data as a function of resistivity and dopant density for temperatures of both 23°C and 300 K. These fits are self-consistent within a few percent so that conversion can go both directions without iteration. Similar analytical expressions were fitted to the calculated hole mobility as a function of resistivity and hole density.

## ACKNOWLEDGMENTS

The authors are indebted to D. R. Ricks for the mechanical four-probe resistivity measurements, to F. H. Brewer for the Hall effect measurements, and to J. Krawczyk and L. A. Robinson for specimen preparation. Special thanks are due M. G. Buehler for designing the test structures used in this work and R. D. Larrabee and W. M. Bullis for helpful comments on the manuscript. The typing of the report with its many tables was expertly done by Jane Walters and Jo Halapatz.

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| <b>4. TITLE AND SUBTITLE</b><br><i>Semiconductor Measurement Technology: The Relationship Between Resistivity and Dopant Density for Phosphorus- and Boron-Doped Silicon</i>   |  |  |  |
| <b>5. AUTHOR(S)</b><br>W. R. Thurber, R. L. Mattis, Y. M. Liu, and J. J. Filliben  |  |  |  |
| <b>6. PERFORMING ORGANIZATION</b> <i>(If joint or other than NBS, see instructions)</i><br><br><b>NATIONAL BUREAU OF STANDARDS</b><br><b>DEPARTMENT OF COMMERCE</b><br><b>WASHINGTON, D.C. 20234</b>   |  | <b>7. Contract/Grant No.</b><br>ARPA Order No. 2397<br>Program Code 7Y10 | <b>8. Type of Report &amp; Period Covered</b><br>Final |
| <b>9. SPONSORING ORGANIZATION NAME AND COMPLETE ADDRESS</b> <i>(Street, City, State, ZIP)</i><br>Defense Advanced Research Projects Agency                      National Bureau of Standards<br>1400 Wilson Boulevard    and                      Washington, DC 20234<br>Arlington, VA 22209  |  |  |  |
| <b>10. SUPPLEMENTARY NOTES</b><br><br>Library of Congress Catalog Card Number 81-600052.<br>Conducted as part of the NBS Semiconductor Technology Program.<br><br><input type="checkbox"/> Document describes a computer program; SF-185, FIPS Software Summary, is attached.  |  |  |  |
| <b>11. ABSTRACT</b> <i>(A 200-word or less factual summary of most significant information. If document includes a significant bibliography or literature survey, mention it here)</i><br>New data have been obtained for the resistivity-dopant density relationship for silicon doped with phosphorus or boron for dopant densities in the range $10^{13}$ to $10^{20}$ $\text{cm}^{-3}$ . For dopant densities less than $10^{18}$ $\text{cm}^{-3}$ , results were calculated from resistivity and junction capacitance-voltage measurements on processed wafers. For more heavily doped material, data were obtained from Hall effect and resistivity measurements on specimens cut from bulk silicon slices. These primary methods were supplemented for phosphorus-doped material by neutron activation analysis and a photometric technique and for boron-doped material by the nuclear track technique. For phosphorus-doped silicon the results of this work differ by 5 to 15 percent from the commonly used Irvin curve, always in the direction of lower resistivity for a given dopant density. For boron-doped silicon the results differ significantly from the <i>p</i> -type Irvin curve for boron densities greater than $10^{16}$ $\text{cm}^{-3}$ with a maximum deviation of 45 percent at $5 \times 10^{17}$ $\text{cm}^{-3}$ in the direction of lower resistivity for a given dopant density. Hole mobility values derived from the data are in reasonable agreement with the Wagner expression with a maximum discrepancy of 10 percent in the $10^{18}$ $\text{cm}^{-3}$ range. Analytical curves were fitted to the resistivity-dopant density product as a function of resistivity and dopant density for temperatures of 23°C and 300 K. Similar curves were obtained for the calculated carrier mobility as a function of resistivity and carrier density. |  |  |  |
| <b>12. KEY WORDS</b> <i>(Six to twelve entries; alphabetical order; capitalize only proper names; and separate key words by semicolons)</i><br>Boron; capacitance-voltage technique; dopant density; electron mobility; Hall effect; hole mobility; Irvin curves; phosphorus; resistivity; semiconductor; silicon.   |  |  |  |
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